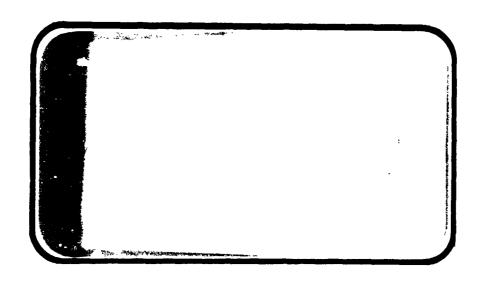


NATIONAL AERONAUTICS AND SPACE ADMINISTRATION



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NASA-CR-134083) EFFECTS OF SURFACE

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CHARACTERISTICS OF THE MODIFIED 089 B

CHARACTERISTICS OF THE

SPACE SHUTTLE

AEROTHERMODYNAMIC DATA REPORT

JOHNSON SPACE CENTER HOUSTON, TEXAS

DATA MANagement services

SPACE DIVISION CHRYSLER
CORPORATION

DMS-DR-2079 NASA CR-134,083

EFFECTS OF SURFACE ROUGHNESS ON THE
AERODYNAMIC CHARACTERISTICS OF THE MODIFIED
089 B SHUTTLE ORBITER AT MACH 6

(LA15)

Ву

George Ashby, Jr., NASA/LaRC

Prepared under NASA Contract Number NAS9-13247

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Data Management Services Chrysler Corporation Space Division New Orleans, La. 70189

for

Engineering Analysis Division

Johnson Space Center
National Aeronautics and Space Administration
Houston, Texas

WIND TUNNEL TEST SPECIFICS

Test Number: LaRC 20" - 6441

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Date: August 13 - September 24, 1973

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FULN. D. Kemp Data Management Services

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EFFECTS OF SURFACE ROUGHNESS ON

THE AERODYNAMIC CHARACTERISTICS OF THE MODIFIED 089 B SHUTTLE ORBITER AT MACH 6 (LA15)

By

George Ashby, Jr.

SUMMARY

A one hundredth scale model of the modified 089B shuttle orbiter was tested in the Langley 20-Inch Mach 6 tunnel. Force and moment, surface pressure and oilflow data were obtained on one model, figure 2a, and phase-change coating data were obtained on another, figure 2b. The pressure tests were conducted first; the tubes were clipped near the base of the model and then the force and moment and oil flow tests conducted. No pressure data or phase change coating results are presented in this report.

Angles of attack for the tests were from 20° to 35° and are commensurate with the range of flight values from entry down to Mach 5. The design flight Reynolds number at Mach 6, based on model length, was 15 x 10^6 , which could not be obtained in the tunnel; therefore, the tests were conducted at the highest and lowest values for this model in the tunnel, 9.4×10^6 and 4.0×10^6 , respectively, to indicate Reynolds number effects. Two control deflection combinations, representative of the bank and pitch control limits of the design flight trajectory, were used. They were $\delta_{\rm e,L} = -10^\circ$, $\delta_{\rm e,R} = 0^\circ$ and $\delta_{\rm e,L} = 14^\circ$, $\delta_{\rm e,R} = 6^\circ$.

The tests were conducted with and without uniformly distributed square roughness pieces to assess the possible effects of raised TPS riles.

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Schedules of Coefficients Plotted

A) CAF, CAB, L/DF, CN, CL vs ALPHA; CDF vs CL; CN, CL vs CLM
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C) DCY/DA, DCYNDA, DCBLDA vs ALPHA

NOMENCLATURE General

l

SYMBOL	SADSAC SYMBOL	DEFINITION
a		speed of sound; m/sec, ft/sec
$C_{\mathbf{p}}$	CP	pressure coefficient; $(p_1 - p_{\infty})/q$
M	MACH	Mach number; V/a
p		pressure; N/m ² , psf
q	Q(NSM) Q(PSF)	dynamic pressure; 1/2pV ² , N/m ² , psf
rn/L	RN/L	unit Reynolds number; per m, per ft
V		velocity; m/sec, ft/sec
α	AL PHA	angle of attack, degrees
β	BETA	angle of sideslip, degrees
Ψ	PSI	angle of yaw, degrees
φ	PHI	angle of roll, degrees
ρ		mass density; kg/m^3 , slugs/ft ³
	Refe	erence & C.G. Definitions
Ab .		base area; m ² , ft ²
b	BREF	wing span or reference span; m, ft
c.g.		center of gravity
A REF	LREF	reference length or wing mean aerodynamic chord; m, ft
S	SREF	wing area or reference area; m2, ft2
	MRP	moment reference point
	XXRP	moment reference point on X exis
	DR P	moment reference point on Y exis
	20CP	moment reference point on Z exis
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ь 1		base local
В		static conditions
t es		total conditions free stresm

NOMENCLATURE (Condinued)

Body-Axis System

SYMBOL	SADSAC SYMBOL	DEFINITION
$^{\rm C}$ N	C n	normal-force coefficient; normal force qS
c _A	CA	axial-force coefficient; axial force
$c_{\mathbf{Y}}$	C.Z	side-force coefficient; side force qS
$^{C}A_{b}$	CAB	base-force coefficient; base force
		-A _b (p _b - p _w)/qS
c_{Af}	CAF	forebody axial force coefficient, $C_{\mbox{\scriptsize A}}$ - $C_{\mbox{\scriptsize A}b}$
C _m	CLM	pitching-moment coefficient; pitching moment
c_n	CYN	yawing-moment coefficient; yawing moment qSb
c 1	C BL	rolling-moment coefficient; rolling moment
		Stability-Axis System
cr	CL	lift coefficient; lift qS
c_{D}	CD	drag coefficient; drag
$c_{D_{\mathbf{b}}}$	CDB	base-drag coefficient; base drag
$c_{D_{\mathbf{f}}}$	CDF	forebody drag coefficient; CD - CD6
$c_{\mathbf{Y}}$	CY	side-force coefficient; side force qS
C _m	CLM	pitching-moment coefficient; pitching moment
c_n	CLN	yaving-moment coefficient: yaving moment qSb
T.	CSL	rolling-moment coefficient; rolling moment
L/D	L/D	lift-to-drag ratio; C _I /C _D
L/D _f	L/DF	lift to forebody drag ratio; $c_{\rm I}/c_{\rm Df}$

NOMENCLATURE

ADDITIONS TO STANDARD LIST

SYMBOL	DMS SYMBOT.	DEFINITION
$c_{Y_{\vec{\beta}}}$	DCY/DB	side force coefficient derivative with respect to beta, Algebraic difference of the side force coeffi- cient of two runs divided by the algebraic difference of the sideslip angle of the runs; per degree
c _{n,s}	DCYNDB	yawing moment coefficient derivative with respect to beta. Algebraic difference of the yawing moment coefficient of two runs divided by the algebraic difference of the sideslip angle of the two runs; per degree
c _k	DCBLDB	rolling moment coefficient derivative with respect to beta. Algebraic difference of the rolling moment coefficient of two runs divided by the algebraic difference of the sideslip angle of the two runs; per degree.
$^{C_{oldsymbol{Y}_{\delta_{\mathbf{a}}}}}$	DCY/DA	side force coefficient derivative with respect to aileron deflection. Value of side force coefficient with some aileron deflection divided by the value of the aileron deflection; per degree.
$^{C_{n_{\delta_{a}}}}$	DCYNDA	yawing moment coefficient derivative with respect to aileron deflection. Value of yawing moment coefficient with some aileron d flection divided by the value of the aileron deflection; per degree.
$c_{(\delta_{\mathbf{a}})}$	DCBLDA	rolling moment coefficient derivative with respect to aileron deflection. Value of rolling moment coefficient with some aileron deflection divided by the value of the aileron deflection; per degree.
⁵ e	ELEVTR	elevator deflection angle, degrees $(\delta_{eL} + \delta_{eR})/2$; positive trailing edge down.
[§] a	AILRON	aileron deflection angle, degrees; $(\delta_{e_L} - \delta_{e_R})/2$; positive left trailing edge down.
$^{\delta}$ eL	ELVN-L	left elevon deflection angle, degrees
⁸ eR	ELVN-R	right elevon deflection angle, degrees

NOMENCLATURE ADDITIONS TO STANDARD LIST (Cont.)

SYMBOL	DMS SYMBOL	DEFINITION
^S r	RUDDER	rudder deflection angle, degrees, positive trailing edge left
⁸ RF	RUDFLR	rudder flare angle, degrees; for split rudder, included angle/2.
	RGHNSS	parameter name for vehicle surface roughness; value 0.0 indicates no roughness, value 1.0 indicates roughness present.

TEST FACILITY DESCRIPTION

The LaRC 20-inch Mach 6 Tunnel is a blowdown type using air from a 600 psi tank field which is heated by electrical resistance heaters to obtain the desired test conditions. The test Mach number is achieved with a fixed geometry two-dimensional contour nozzle with parallel side walls. The throat is 0.339 x 20.0 inches and the test section, 89.4 inches downstream of the throat, is 20.5 x 20.0 inches. The model was installed with booster centerline at the centerline of the test section, which from previous tests was shown to have a uniform test core of 6.8 x 10 inches at the booster nose and increasing to 12 x 13 inches near the tail.

TEST CONDITIONS

An attempt was made to size the roughness according to the boundary layer properties. In this regard, the boundary layer displacement thicknesses were calculated normal to the wing leading edge using the program developed by Hixon, Beckwith and Bushnell in NACA TMX-2140. Calculated values at both flight and wind tunnel conditions for Mach 6 were found to vary according to the geometric scale of the flight and tunnel models. Similarly, values of boundary layer thickness parameters calculated by Hamilton for the forebody using the methods of AIAA paper 72-703 were found to scale in the same manner. Roughness heights required for transition on the tunnel molel wing were computed from North American Aviation Report AFOSR TN60-1164 by Van Driest and Blumer using the displacement thicknesses computed above. These roughness heights (.003" on upper surface and .0015" on lower surface) were larger than the anticipated differences in TPS tile height (.0007") on the wind tunnel model. Since the calculated roughness heights for transition were higher than the expected surface irregularities, an available roughness thickness (.008) was used on all surfaces for convenience and to provide some boundary-layer tripping margin so that the effects of roughness on aerodynamic performance could be determined. Roughness placement is shown in figure 3.

The classical turbulent wedge (see e.g. NASA TMS-2146) was observed behind the placed roughness on the bottom of the body only. No such patterns were apparent on the leeward surfaces or on the bottom wing surface. The .008 roughness was more than sufficient to trip the boundary layer in

the case cited; epoxy residue and surface irregularities, .001" to .003", near the roughness locations caused the turbulent patterns to appear on the body lower surface with the roughness removed. The distance from the roughness element to transition varies inversely with roughness location relative to the longitudinal centerline of the body and is consistent with the trend observed by Morrisette at Langley on a similar model in the same tunnel.

EXPERIMENTAL RESULTS

Neither roughness, sideslip nor Reynolds number was found to have a significant effect on the longitudinal aerodynamic coefficients of the configuration at Mach 6 (see appropriate figures). Therefore assuming that roughness at the highest Reynolds number of the tests is representative of the conditions in flight, one would not expect the aerodynamic performance to be affected by differences in tile height up to an order of magnitude larger than the design tolerances.

Roughness did, however, have an observable effect on the lateral aerodynamic coefficients for up aileron (only side force was strongly affected with down aileron). For the up aileron case, the side force was reduced and the roll and yaw were increased by roughness. These effects are noted to be reduced as Reynolds number is increased (compare control effectiveness plots for the two Reynolds numbers of the tests) and at flight conditions should be less than shown by the data at our highest Reynolds number. Oil flows at $\alpha = 20^{\circ}$ with aileron up show only slight changes in the surface flow patterns over both the windward and leeward surfaces when roughness

was added. Examination of the surface pressure measurements, however, shows that roughness effects on the roll and yaw are caused by quasi-uniform changes in pressure over both surfaces of the wing and elevon. For up aileron the pressure on the upper surface is increased about half as much as the pressure is reduced over the lower surface. The two changes together cause an overall increase in roll effectiveness and in yaw. For down aileron, however, the pressure in general is reduced over the upper surface as well as on the lower surface, which reduces the roughness effect on roll and yaw. The effect of roughness on side force and yaw are not totally discernable in the pressure distribution over the upper and lower surfaces because the body side pressure and center of pressure variation due to roughness influence those two parameters.

Lateral and directional stability also reflect the effect of roughness. The effect tends to increase with Reynolds number and, therefore, may be larger at flight conditions. The effects of roughness on these stabilities, however, are observed to be nearly constant over the angle of attack range, making it somewhat easier to correct with augmentation.

No hysteresis effects of boundary-layer separation and reattachment were observed in the data when points were repeated by traversing the angle of attack range from the opposite direction.

DATA REDUCTION

Six component force and moment data recorded by the internal strain gauge balance were reduced to coefficient form using standard data reduction procedures. Reference dimensions used were:

 S_{REF} = wing planform area = 38.736 sq. in.

 $\ell_{REF} = \bar{c} = \text{wing mean aerodynamic chord} = 4.748 \text{ inches}$

 b_{REF} = wing span = 9.367 inches

Moments are about a reference c.g. location 8.507 inches aft of the model nose.

Base pressure measurements were recorded and used to determine a base axial force coefficient, which was applied as a correction to balance recorded axial force.

CONCLUDING REMARKS

The purpose of this investigation was to determine the variation of aerocynamic performance and stability and control of the 089B Shuttle Orbit?r with changes in boundary-layer characteristics resulting from TPS tile height differences on the vehicle in flight. To do this, the wind tunnel data at Mach 6 for the configuration without roughness were compared with data for the configuration with discrete roughness squares paralled to and near the wind leading edge and on the forward part of the body. The roughness squares were scaled according to the TPS tile size and had a height that was an order of magnitude greater than the tolerance for tile height difference.

Boundary-layer type

The boundary-layer calculation for the body portion, using the shuttle criteria for transition, indicated that natural transition would occur in flight on the lower surface at Mach 6 near the placed roughness

squares but would not occur in the wind tunnel at 2/3 flight Reynolds number. In the wind tunnel test at 2/3 flight Reynolds number, however, roughness particles and surface irregularities slightly larger than anticipated tile height differences tripped the boundary layer. Therefore, transition is expected to occur on the body lower surface in flight at Mach 6 with or without tile height variations.

No transition criteria was applied to the boundary-layer calculations for the wing, and the wind tunnel results with roughness squares do not show transition at 2/3 flight Reynolds number. Therefore, the wing boundary-layer is expected to be laminar in flight at Mach 6 on a smooth model. Whether tile height difference will trip the wing boundary-layer in flight is not answered by these tests.

Longitudinal aerodynamics

For up aileron the control effectiveness was, in general, increased by roughness. However, the effect is reduced as Reynolds number is increased from 1/4 to 2/3 of full scale and, if the trend continues, would be minimal at flight Reynolds numbers. For down aileron the effect of roughness is insignificant at all Reynolds numbers.

Lateral and directional stability

The effect of roughness on lateral and directional stability is insignificant at Reynolds number 1/4 of full scale; however, roughness reduces both stabilities at 2/3 of full scale Reynolds number and, if the trend continues, could become significant at full scale. The effect is uniform with angle of attack, however, making it somewhat easier to correct with augmentation.

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axes have been displaced from the center For clarity, origins of wind and stability 1. Positive directions of force cofficients, moment coefficients, and angles are indicated by arrow of gravity Notes 2.

Figure 1. - Axie Systems.

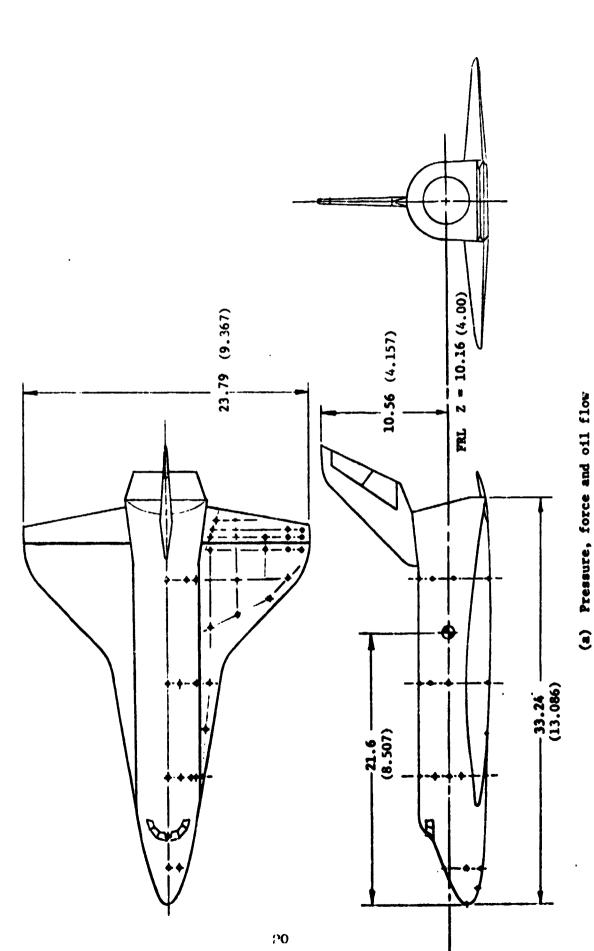
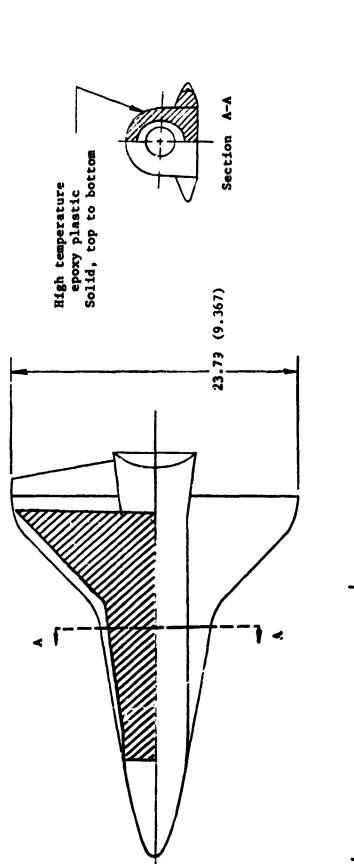
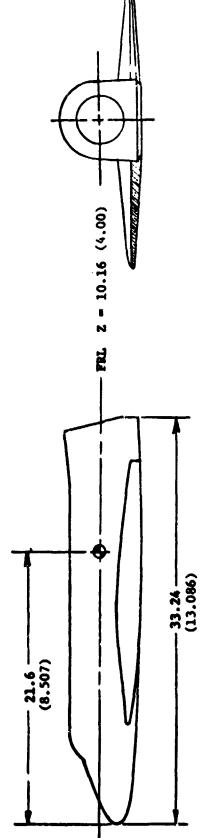


Figure 2.- One-hundredth scale model of modified 089B shuttle orbiter showing orifice locations. All cimensions in centimeters (Inches)



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(b) Piase change coatings

Figure 2.- Concluded.

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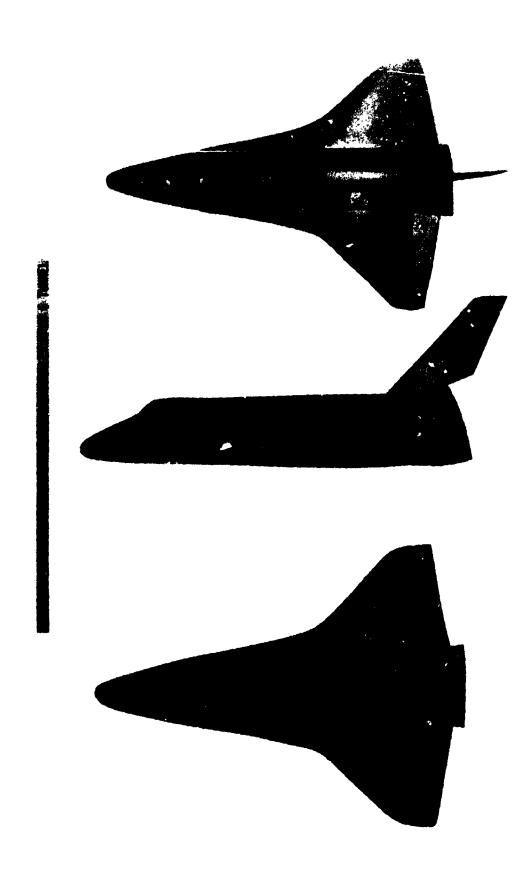
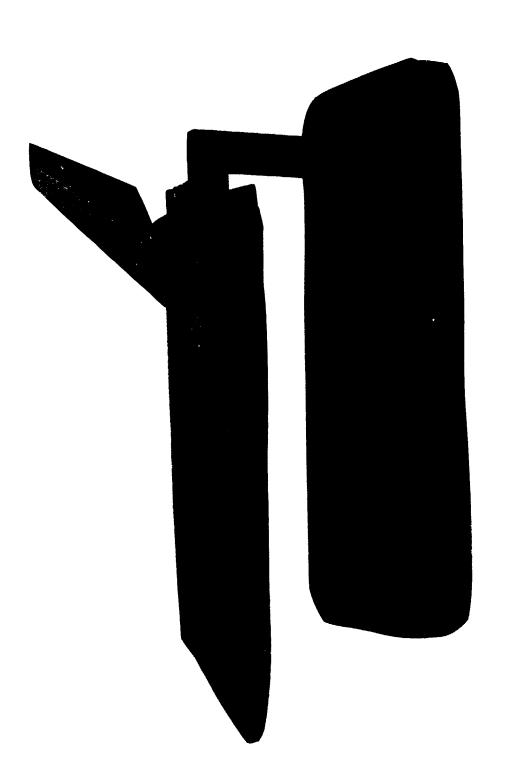


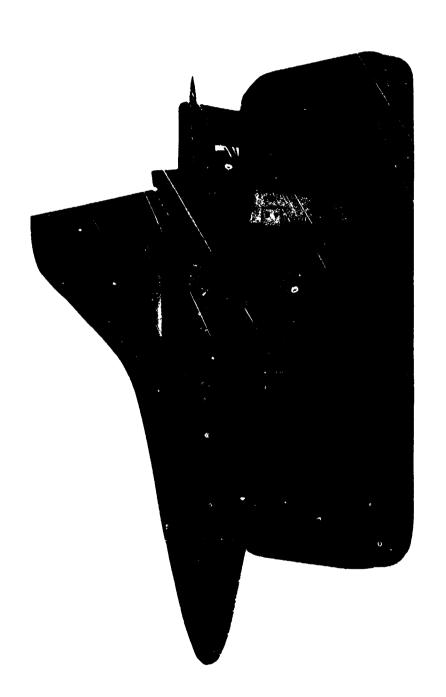
FIGURE 3. ROUGHNESS LOCATIONS ON 089B URBITER IN LANGLEY MACH 6 TUNNEL

DATA FIGURES



.01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION SHOWING LOCATIONS OF .0625" x .0625" x .008" ROUGHNESS SQUARES FIGURE 1.

A. SIDE VIEW



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FIGURE 1. (CONTINUED)

B. TOP VIEW

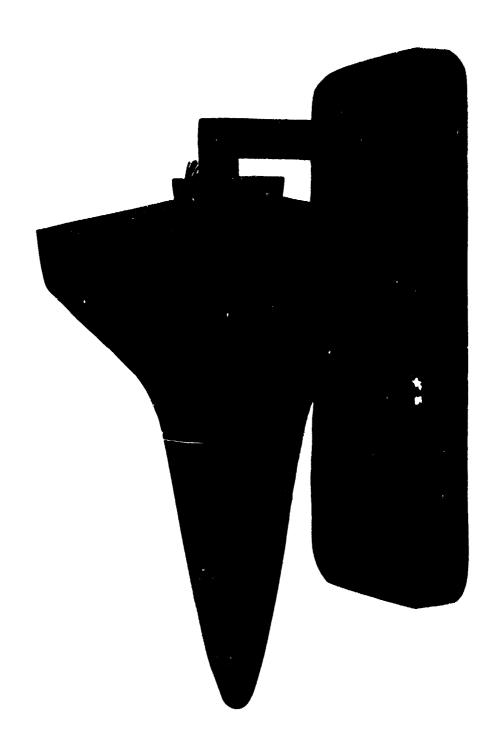
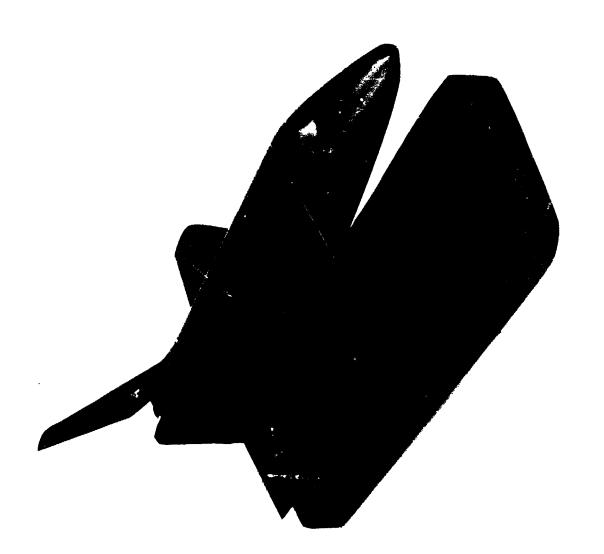


FIGURE 1. (CONTINUED)

C. BOTTOM VIEW

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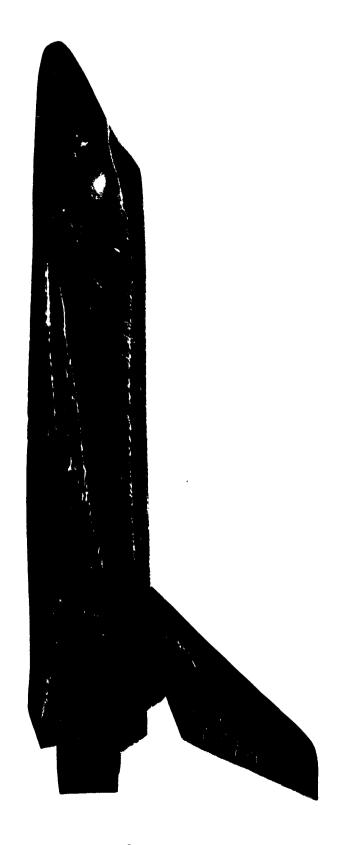


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FIGURE 1. (CONTINUED)

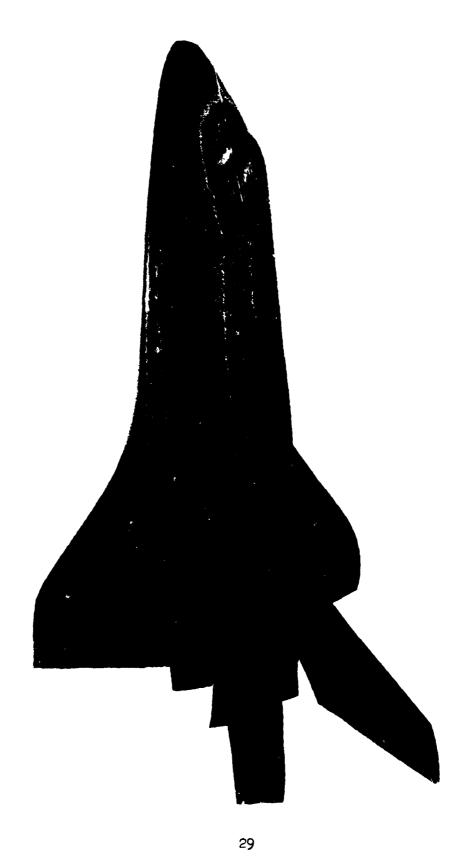
D. FRONT-OBLIQUE VIEW



OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT α = 20°, β = 0°, $\delta_{\rm eL}$ = -10°, $\delta_{\rm eR}$ = 0, RN/L = 9.4 \times 106, ROUGHNESS OFF FIGURE 2.

A. LEFT SIDE VIEW

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B. LEFT WING-BODY JUNCTION VIEW FIGURE 2. (CONTINUED)

FIGURE 2. (CONTINUED)
C. TOP VIEW

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FIGURE 2. (CONTINUED)
D. RIGHT WING-BODY JUNCTION VIEW

31

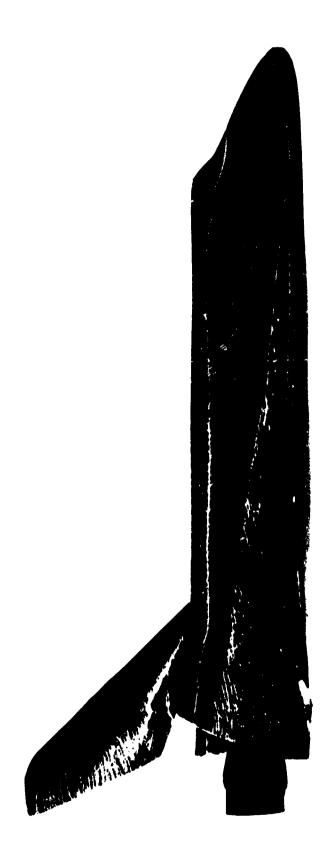


FIGURE 2. (CONTINUED)

E. RIGHT SIDE VIEW

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FIGURE 2. (CONTINUED) F. BOTTOM VIEW

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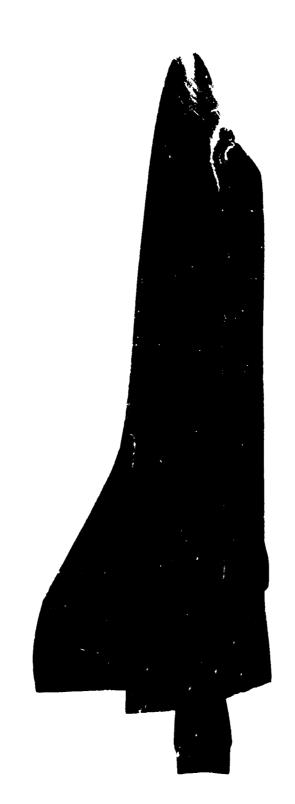
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FIGURE 3. OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT $\alpha = 20^\circ$, $\beta = 0^\circ$, $\delta_{eL} = -10^\circ$, $\delta_{eR} = 0$, RN/L = 9.4 x 106, ROUGHNESS ON

A. LE. SIDE VIEW

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FIGURE 3. (CONTINUED)

B. LEFT WING-BODY JUNCTION VIEW

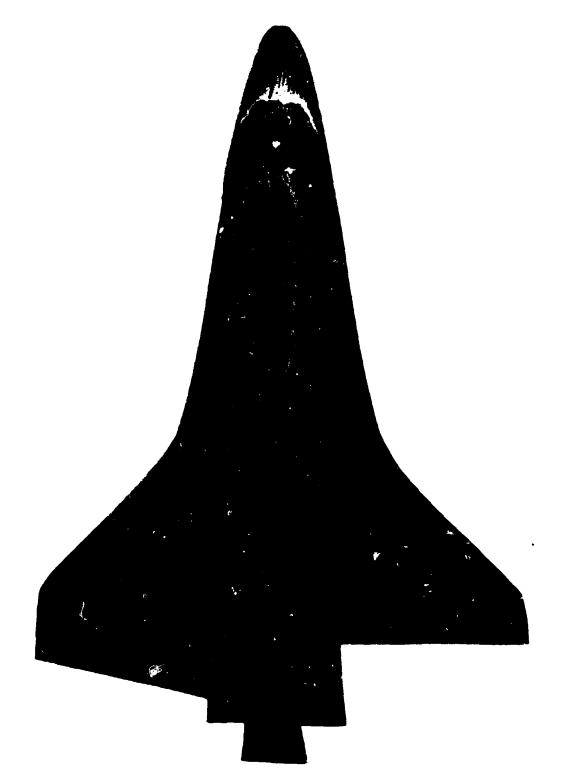
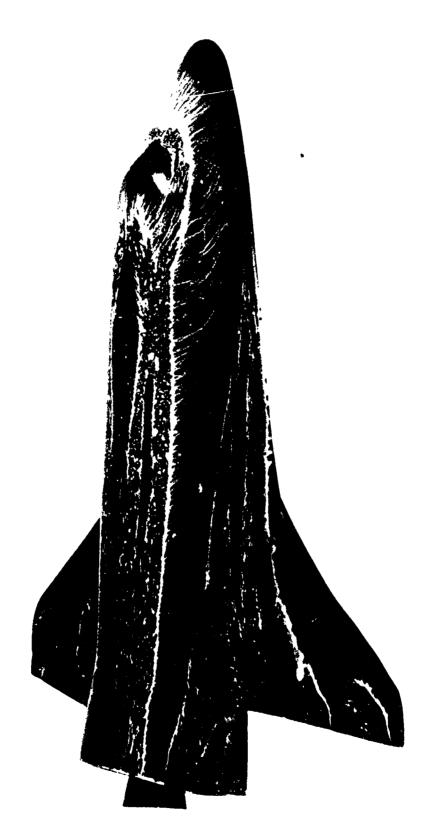


FIGURE 3. (CONTINUED)

C. TCP VIEW



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FIGURE 3. (CONTINUED)

D. RIGHT WING-BODY JUNCTION VIEW

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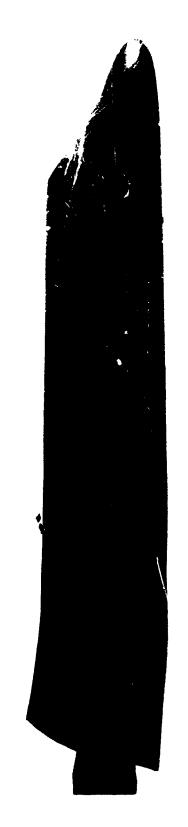
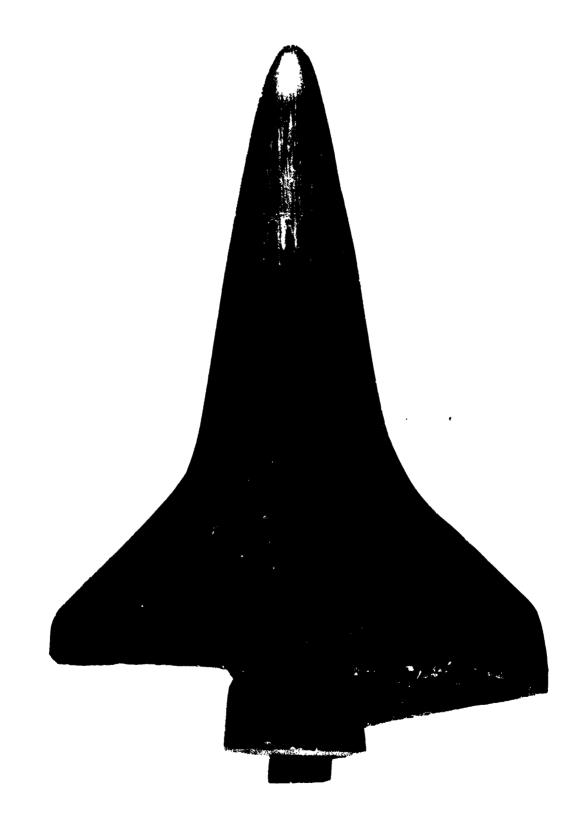


FIGURE 3. (CONTINUED)

E. RIGHT 'DE VIEW



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FIGURE 3. (CONTINUED)

F. BOTTOM VIEW

FIGURE 4. OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT $\alpha=20^\circ$, $\beta=-5^\circ$, $\delta_{eL}=-10^\circ$, $\delta_{eR}=0^\circ$, RN/L = 9.4 x 10^6 , ROUGHNESS OFF

A. LEFT SIDE VIEW

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B. LEFT WING-BODY JUNCTION VIEW

FIGURE 4. (CONTINUED)

FIGURE 4. (CONTINUED) C. TOP VIEW

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D. RIGHT WING-BODY JUNCTION VIEW

43

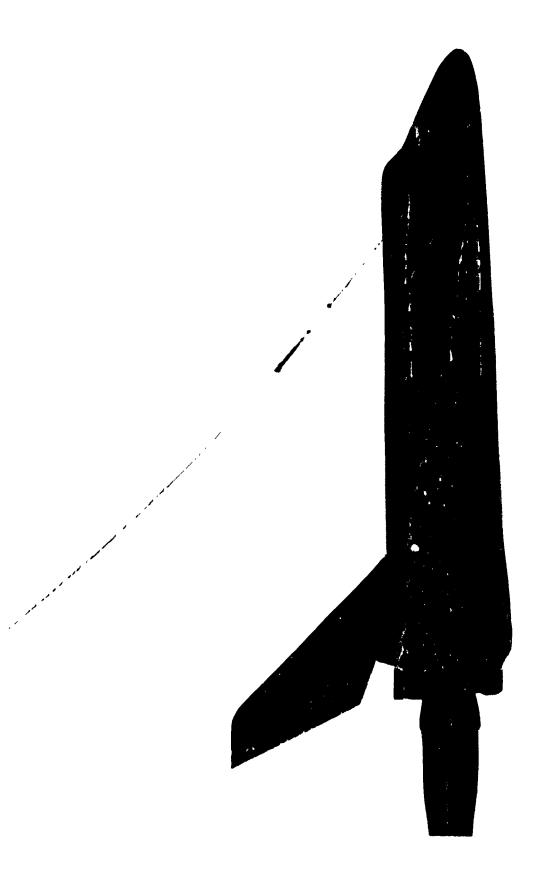


FIGURE 4. (CONTINUED)

E. RIGHT SIDE VIEW

FIGURE 4. (CONTINUED) F. BOTTOM VIEW 45

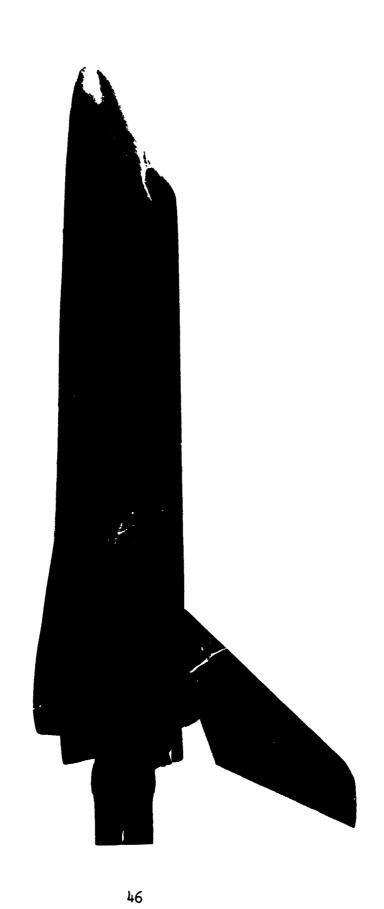


FIGURE 5. OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT $\alpha = 20^{\circ}$, $\beta = -5^{\circ}$, $\delta_{eL} = -10^{\circ}$, $\delta_{eR} = 0^{\circ}$, $RN/L = 9.4 \times 10^{\circ}$, ROUGHNESS ON

A. LEFT SIDE VIEW

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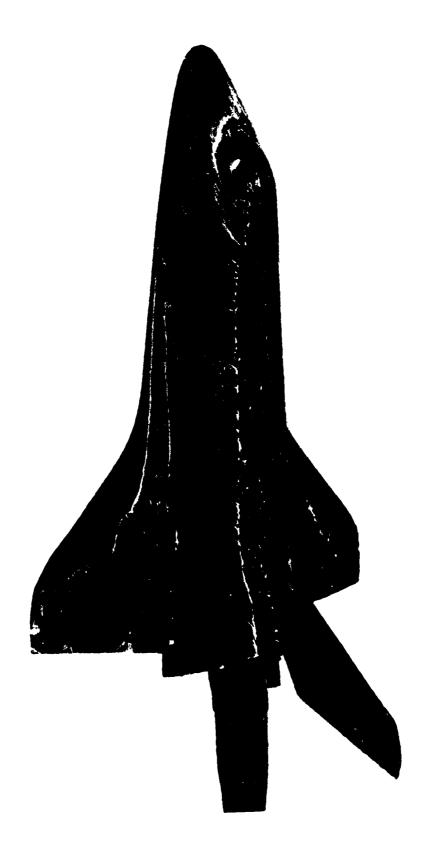


FIGURE 5. (CONTINUED)

B. LEFT WING-BODY JUNCTION VIEW

FIGURE 5. (CONTINUED) C. TOP VIEW

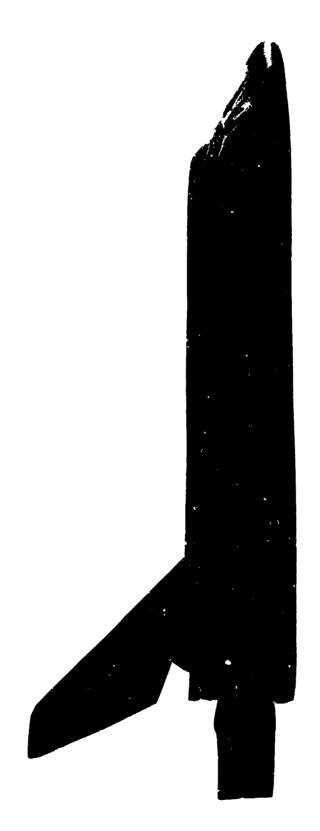
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FIGURE 5. (CONTINUED)

D. RICHT WING-BODY JUNCTION VIEW

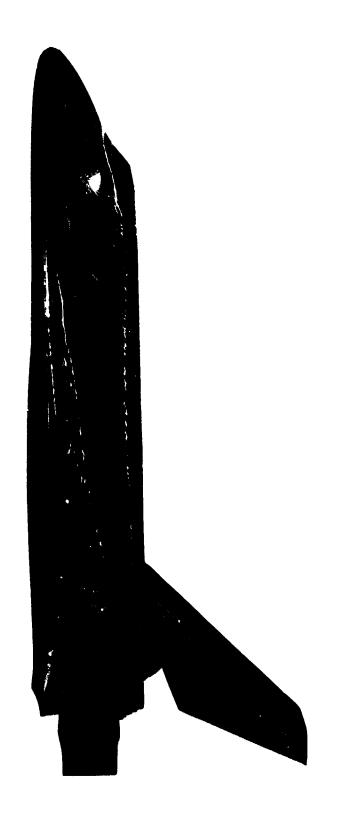


(CONTINUED)

E. RIGHT SIDE VIEW

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FIGURE 5. (CONTINUED) F. BOTTOM VIEW



OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT $\alpha=20^\circ$, $\beta=0^\circ$, $\delta_{eL}=14^\circ$, $\delta_{eR}=6^\circ$, RN/L = 9.4 x 10^6 , ROUGHNESS OFF FIGURE 6.

A. LEFT SIDE VIEW

FIGURE 6. (CONTINUED)

B. LEFT WING-BODY JUNCTION VIEW

FIGURE 6. (CONTINUED)

C. TOP VIEW

FIGURE 6. (CONTINUED)

D. RIGHT WING-BODY JUNCTION VIEW

A SHAPPING

FIGURE 6. (CONTINUED)

E. RIGHT SIDE VIEW

FIGURE 6. (CONTINUED) F. BOTTOM VIEW 57

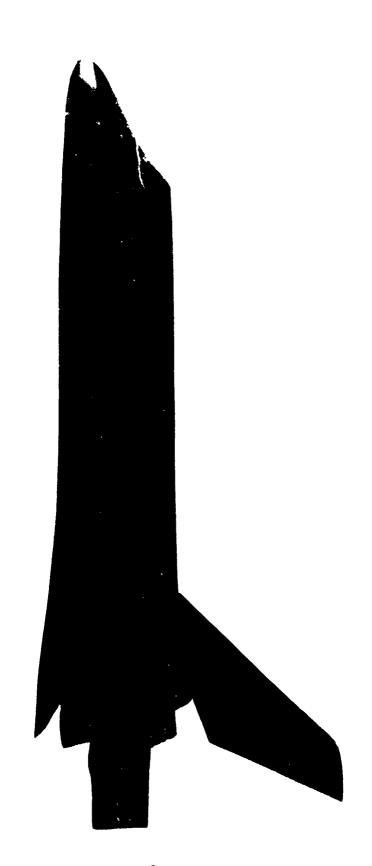


FIGURE 7. OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT $\alpha = 20^\circ$, $\beta = -5^\circ$, $\delta_{eL} = 14^\circ$, $\delta_{eR} = 6^\circ$, RN/L = 9.4 x 10°, ROUGHNESS OFF

A. LEFT SIDE VIEW

FIGURE 7. (CONTINUED)

B. LEFT WING-BODY JUNCTION VIEW

FIGURE 7. (CONTINUED)
C. TOP VIEW

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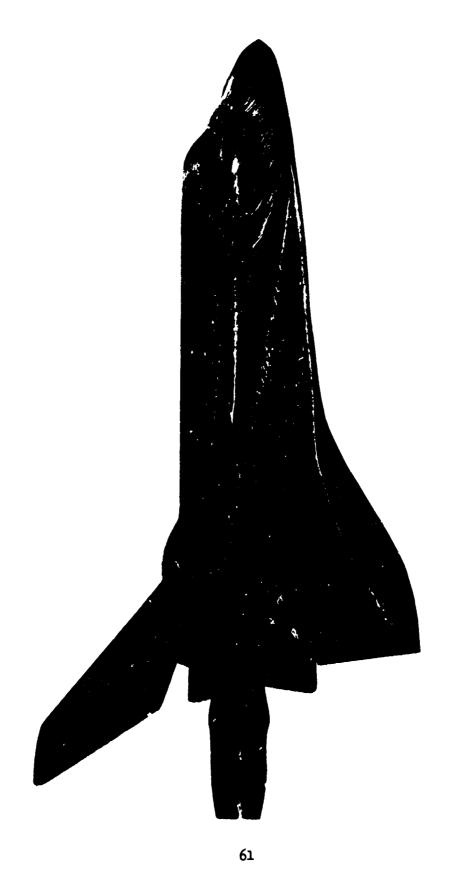


FIGURE 7. (CONTINUED)

D. RIGHT WING-BODY JUNCTION VIEW

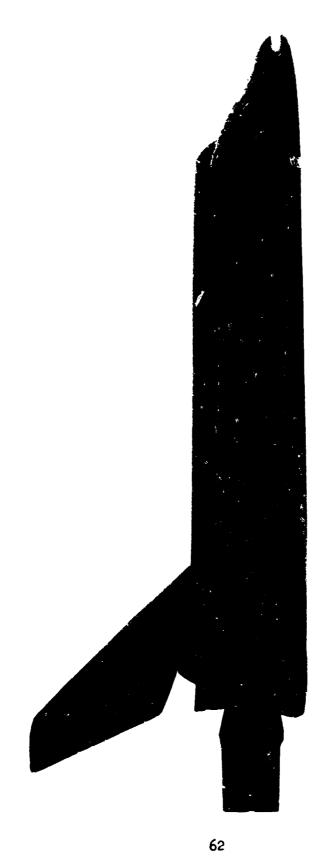


FIGURE 7. (CONTINUED)

E. RICHT SIDE VIEW

FIGURE 7. (CONTINUED) F. ROTTOM VIEW

OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT α = 20°, 6 = 0°, 6eL = 6eR = -30°, RN/L = 9.4 × 106, ROUGHNESS OFF FIGURE 8.

A. LEFT SIDE VIEW

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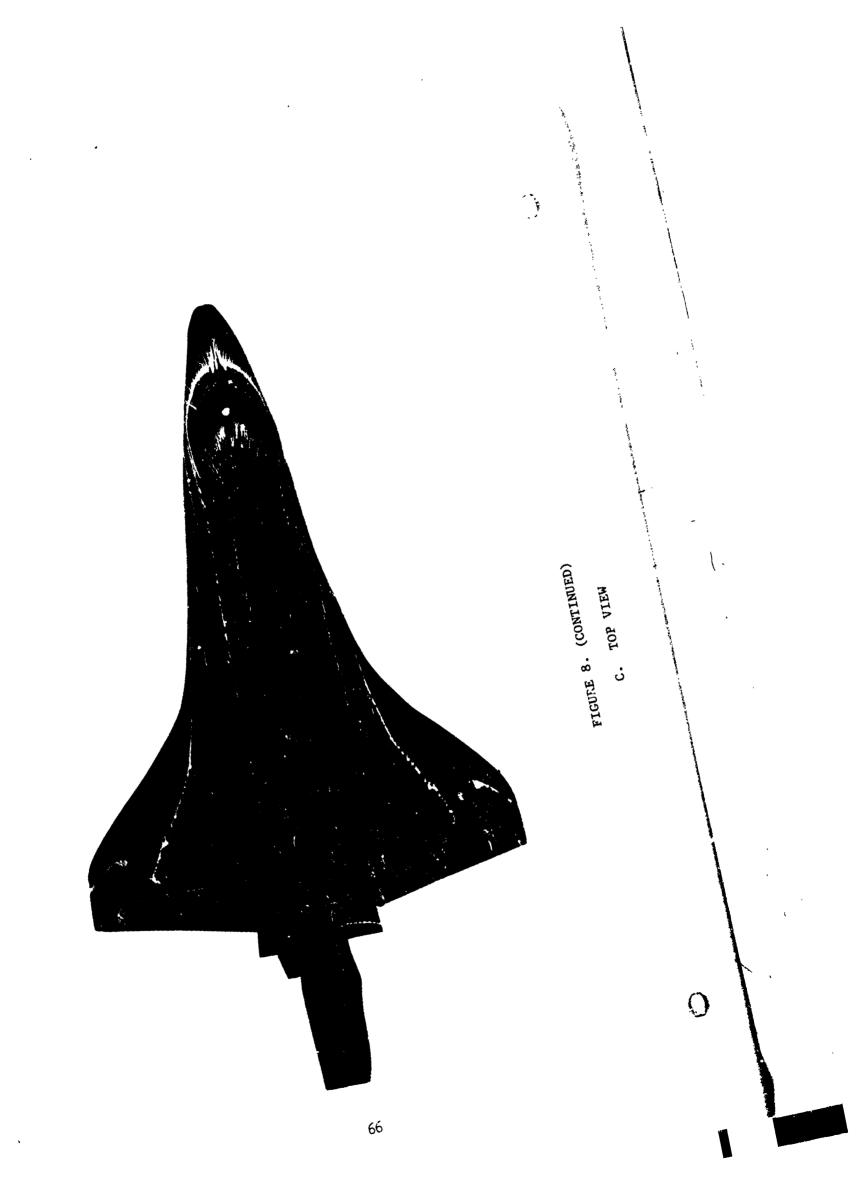
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FIGURE 8. (CONTINUED)

B. LEFT WING-BODY JUNCTION VIEW



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D. RIGHT WING-BODY JUNCTION VIEW

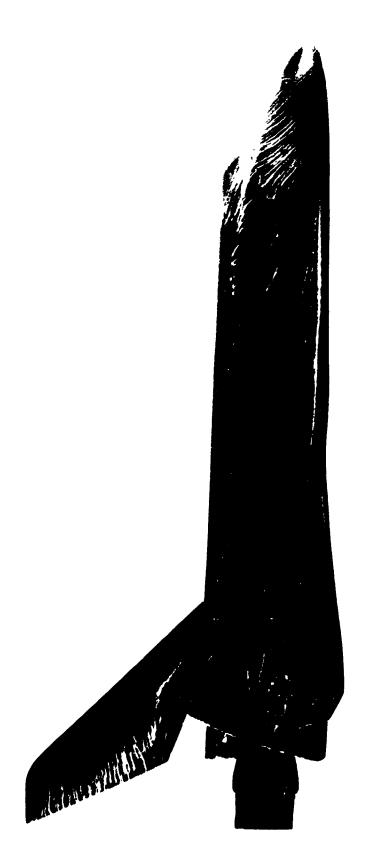


FIGURE 8. (CONTINUED)

E. RIGHT SIDE VIEW

FIGURE 8. (CONTINUED) F. BOTTOM VIEW

OIL FLOW PAITERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT α = 20° β = 0°, $\delta_{\rm eL}$ = -10°, $\delta_{\rm eR}$ = 0°, RN/L = 4.0 x 10⁶, ROUGHNESS OFF FIGURE 9.

A. LEFT SIDE VIEW

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The state of the s

B. LEFT WING-BODY JUNCTION VIEW FIGURE 9. (CONTINUED)

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FIGURE 9. (CONTINUED) C. TOP VIEW



FIGURE 9. (CONTINUED)

D. RIGHT WING-BODY JUNCTION VIEW

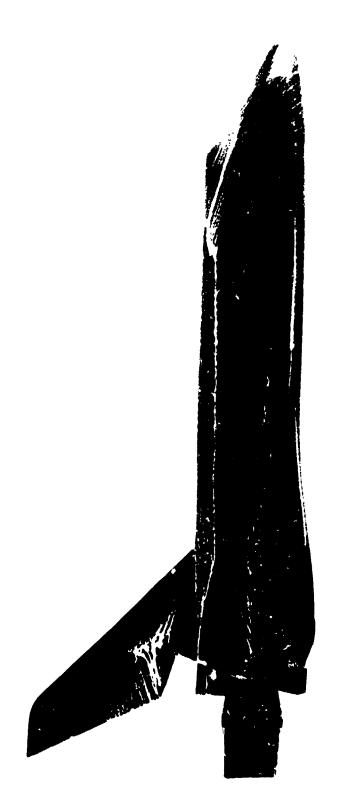
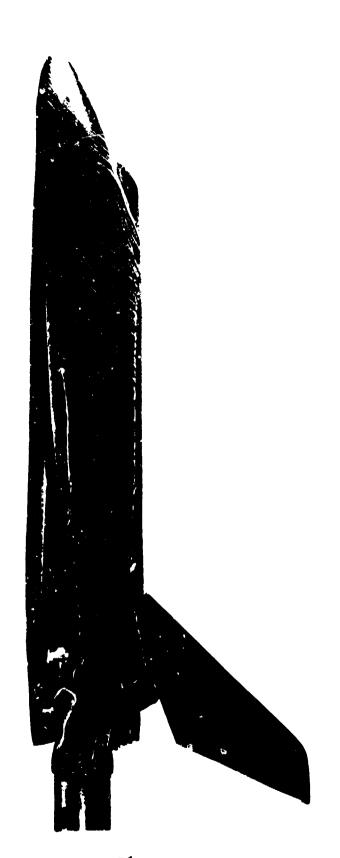


FIGURE 9. (CONTINUED)

E. RIGHT SIDE VIEW

FIGURE 9. (CONTINUED) F. BOTTOM VIEW



OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT α = 20° B = -5°, $\delta_{\rm eL}$ = -10°, $\delta_{\rm eR}$ = 0°, RN/L - 4.0 x 106, ROUGHNESS OFF FIGURE 10.

A. LEFT SIDE VIEW

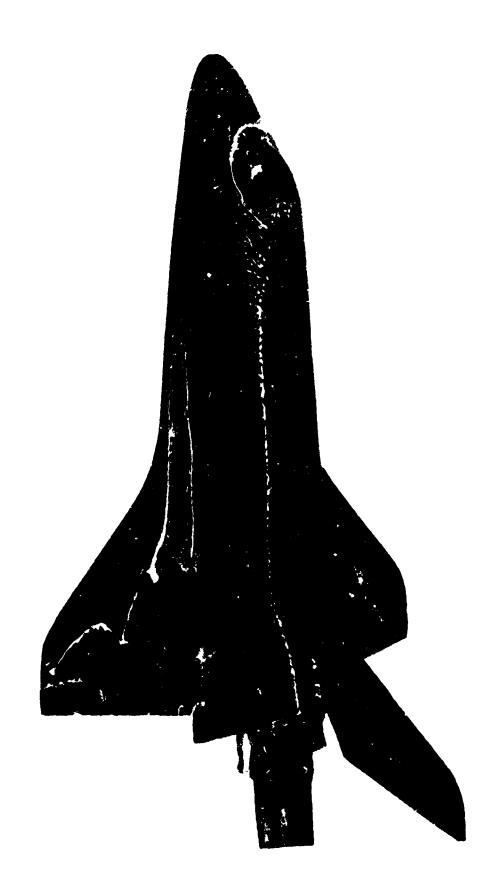


FIGURE 10. (CONTINUED)

B. LEFT WING-BODY JUNCTION VIEW

FIGURE 10. (CONTINUED) C. TOP VITY

FIGURE 10. (CONTINUED) D. RIGHT WING-BODY JUNCTION VIEW

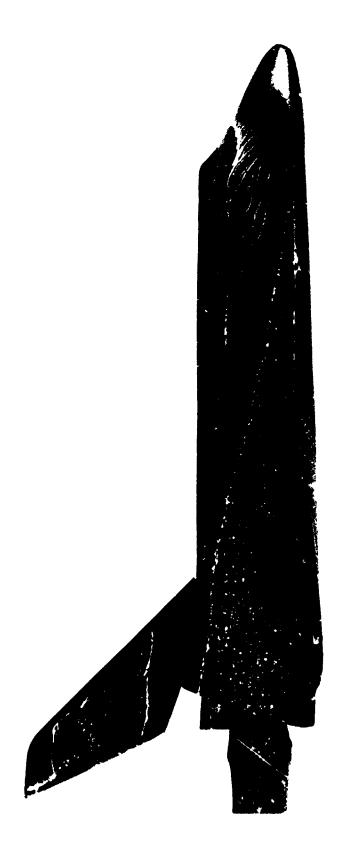


FIGURE 10. (CONTINUED)

E. RIGHT SIDE VIEW

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FIGURE 10. (CONTINUED)
F. BOTTOM VIEW

OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT $_{\alpha}$ = 20°, $_{6}$ = 0°, $_{6}$ = 14°, $_{6}$ er = 6°, RN/L = 4.0 x 10⁶, ROUGHNESS OFF FIGURE 11.

A. LEFT SIDE VIEW

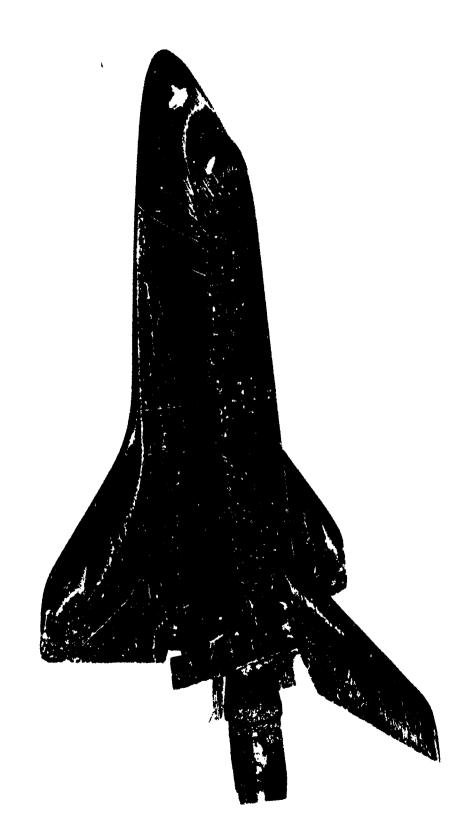


FIGURE 11. (CONTINUED)

B. LEFT WING-BODY JUNCTION VIEW

FIGURE 11. (CONTINUED)
C. TOP VIEW

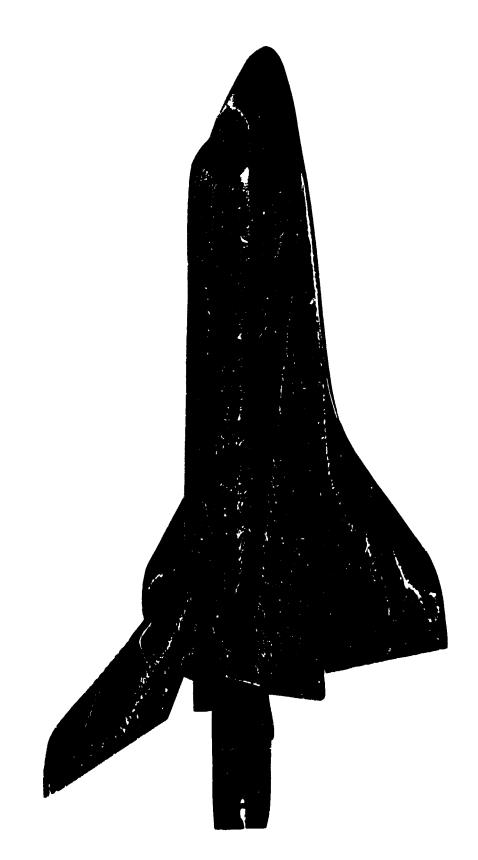


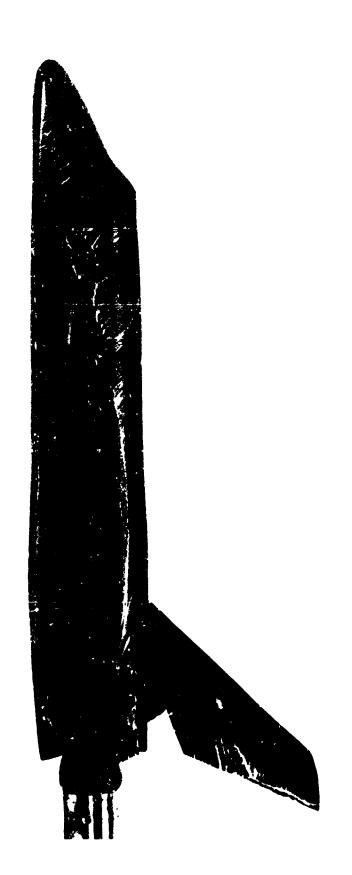
FIGURE 11. (CONTINUED)

D. RIGHT WING-BODY JUNCTION VIEW

FIGURE 11. (CONTINUED)

E. RIGHT SIDE VIEW

FIGURE 11. (CONTINUED) F. BOTTOM VIEW



OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT $\alpha = -25^{\circ}$, $\beta = 0^{\circ}$, $\delta_{eL} = \delta_{eR} = -30^{\circ}$, RN/L = 4.0 x 10⁶, ROUGHNESS OFF FIGURE 12.

A. LEFT SIDE VIEW

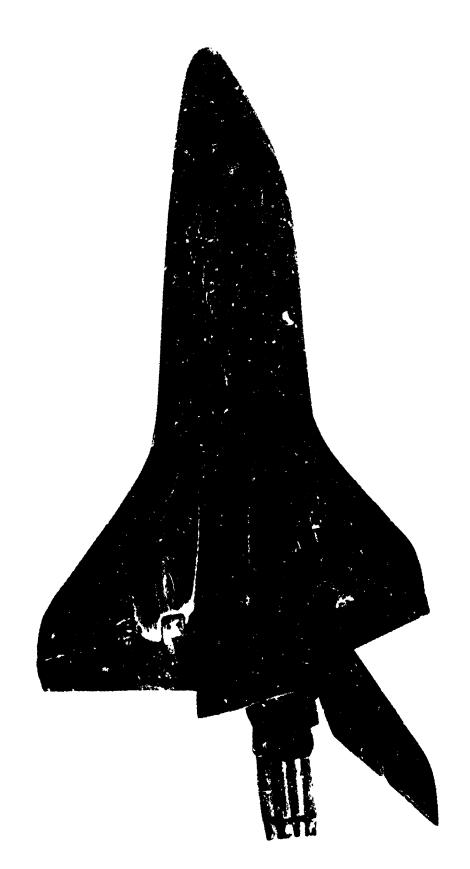


FIGURE 12. (CONTINUED)

FIGURE 12: B. LEFT WING-BODY JUNCTION VIEW FIGURE 12. (CONTINUED) C. TOP VIEW

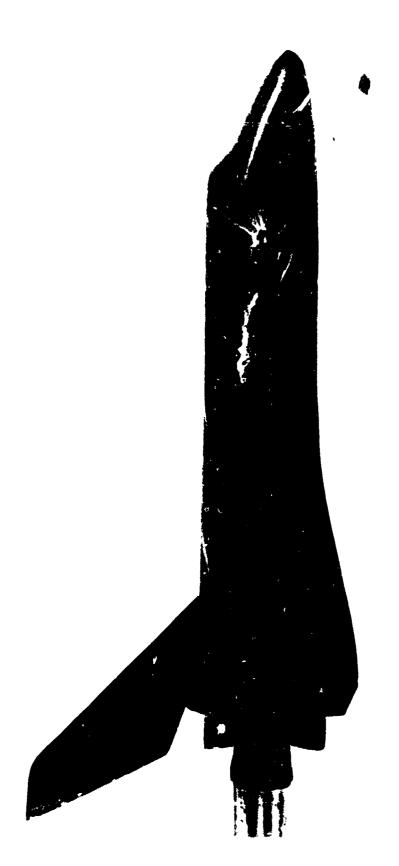
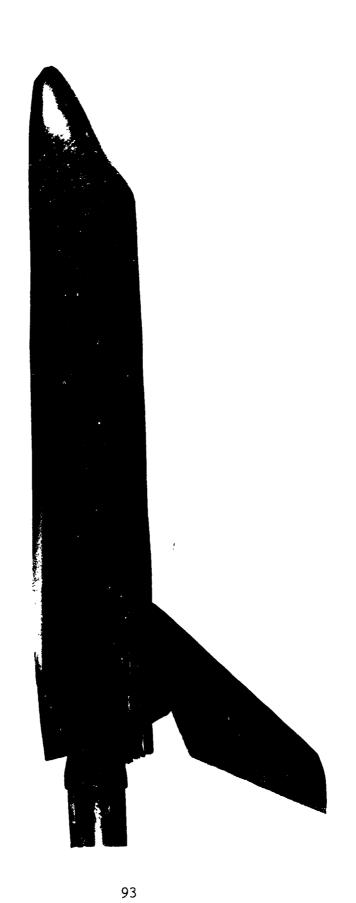


FIGURE 12. (CONTINUED)

D. RIGHT SIDE VIEW

FIJURE 12. (CONTINUED) E. ROTTOM VIEW



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FIGURE 13. OIL FLOW PATTERNS ON THE .01 SCALE MODIFIED ROCKWELL (089B) ORBITER CONFIGURATION AT $\alpha = -25^{\circ}$, $\beta = +5^{\circ}$, $\delta_{eL} = \delta_{eR} = -30^{\circ}$, RN/L = 4.0 x 10⁶, ROUGHNESS OFF

A. LEFT SIDE VIEW

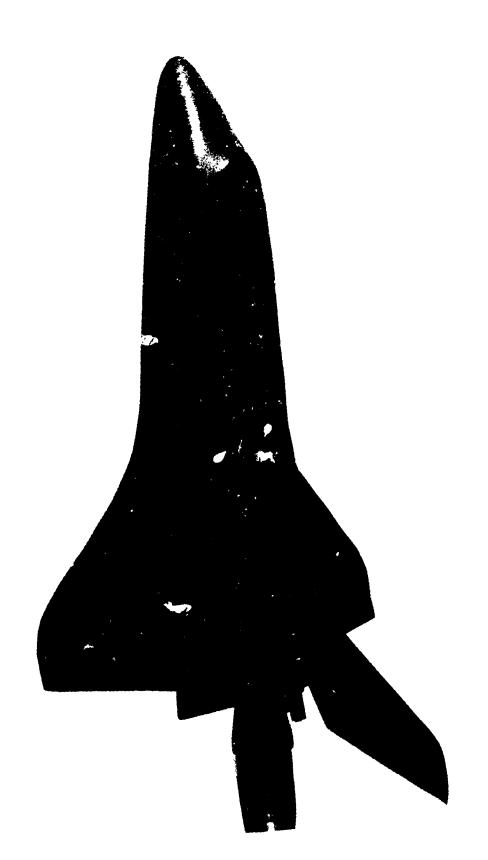


FIGURE 13. (CONTINUED)

B. LEFT WING-BODY JUNCTION VIEW

FIGURE 13. (CONTINUED) C. TOP VIEW

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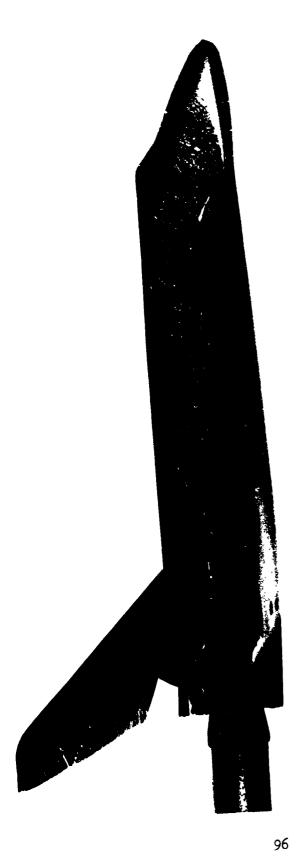


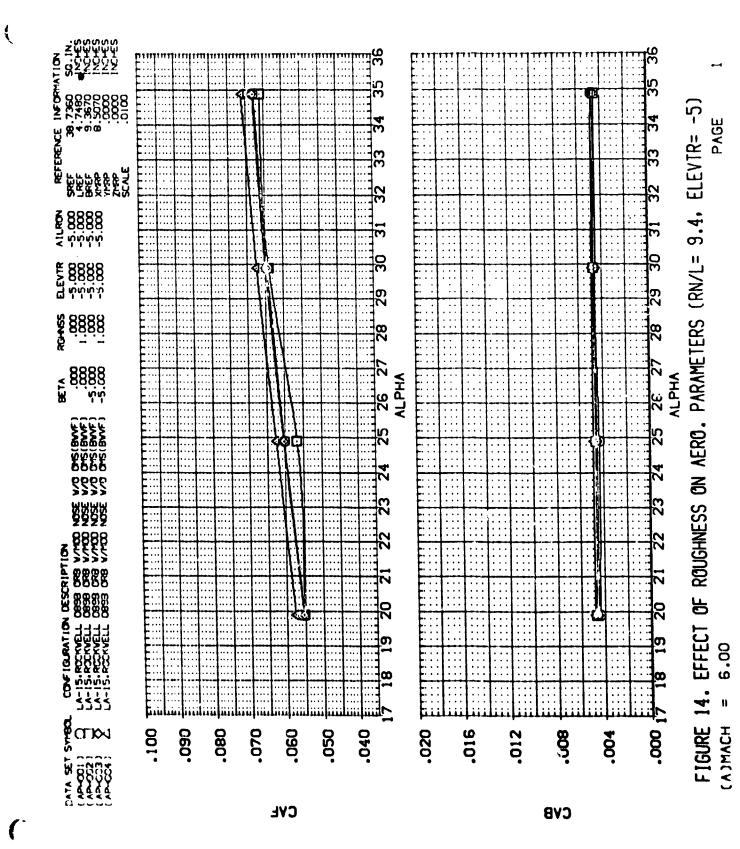
FIGURE 13. (CONTINUED)

D. RIGHT SIDE VIEW

FIGURE 13. (CONTINUED) E. BOTTOM VIEW

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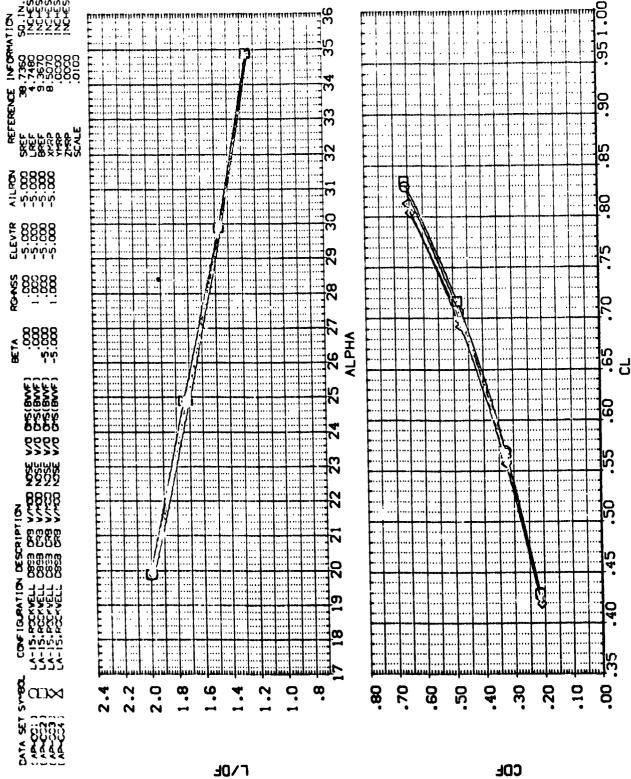
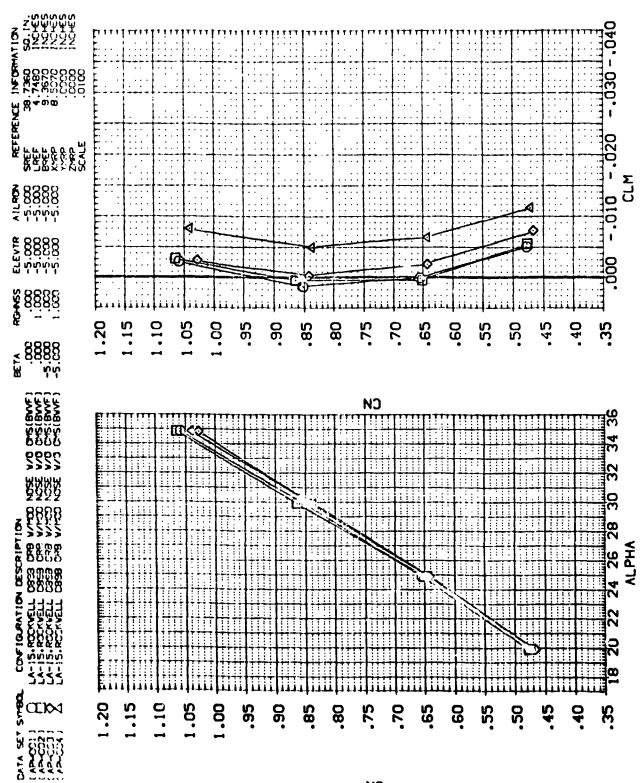


FIGURE 14. EFFECT OF ROUGHNESS ON AERO. PARAMETERS (RN/L= 9.4. ELEVIR= -5) 6.00

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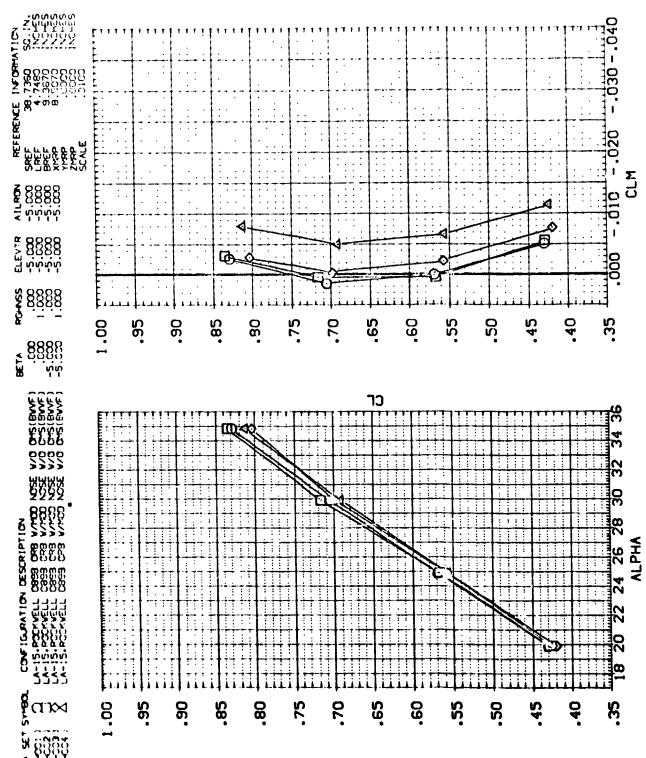
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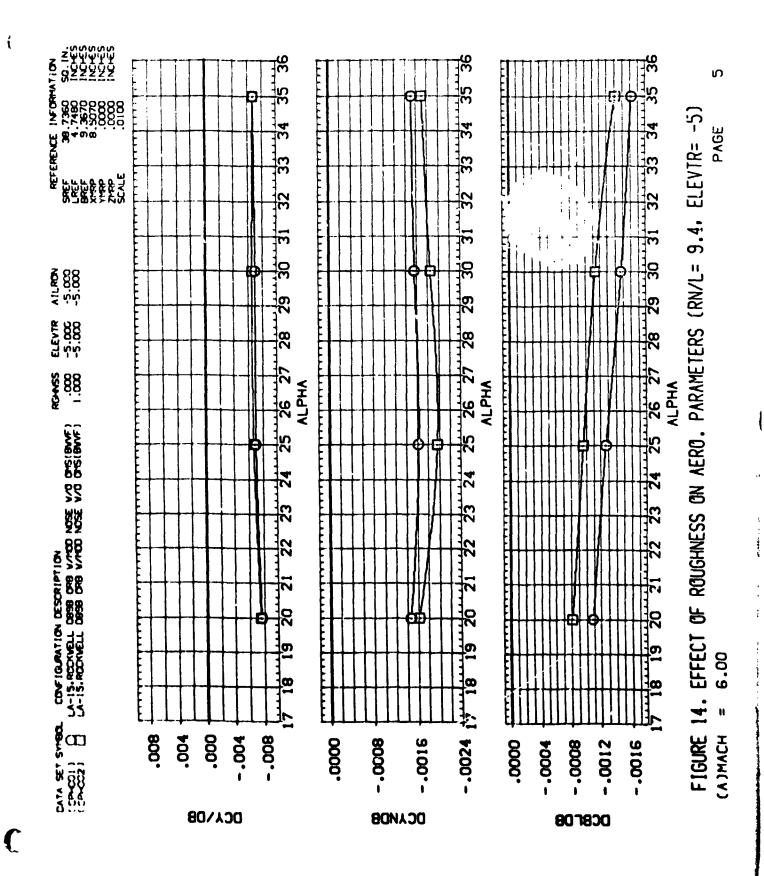
9.4, ELEVTR= -5) PAGE OF ROUGHNESS ON AERO. PARAMETERS (RN/L= EFFECT 6.00 14. FIGURE (A)MACH

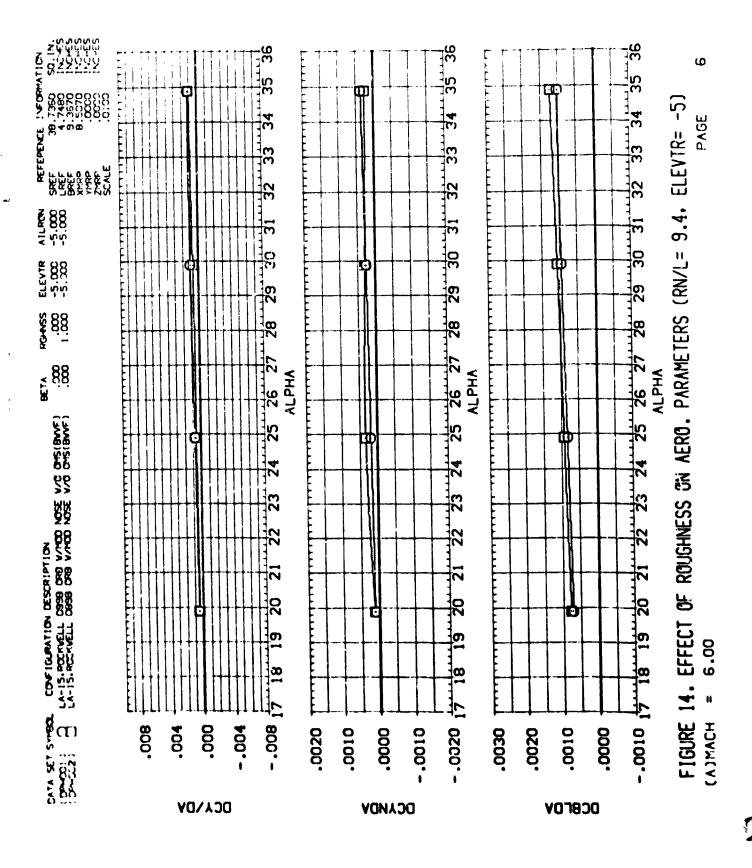
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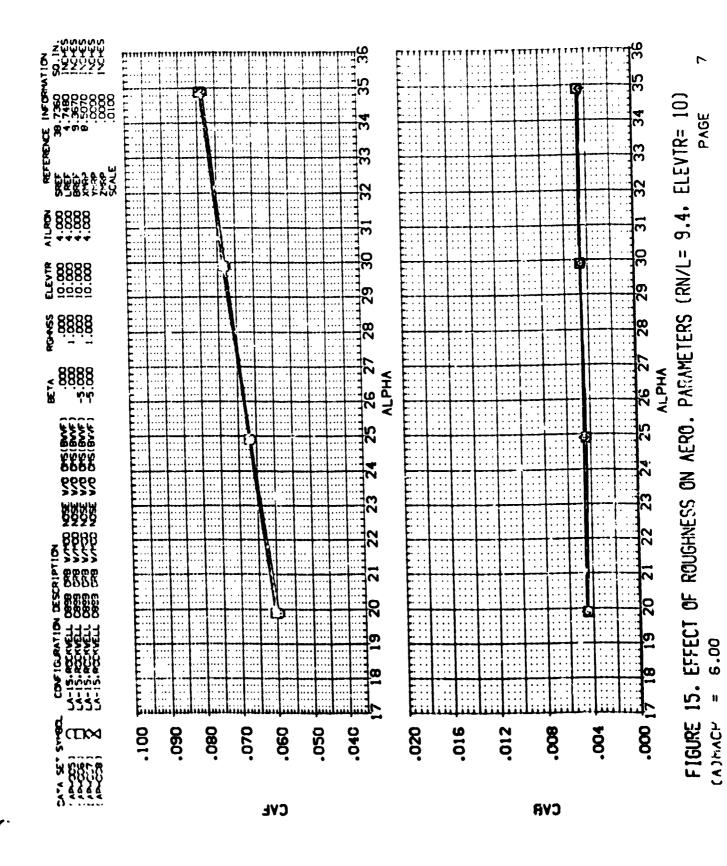
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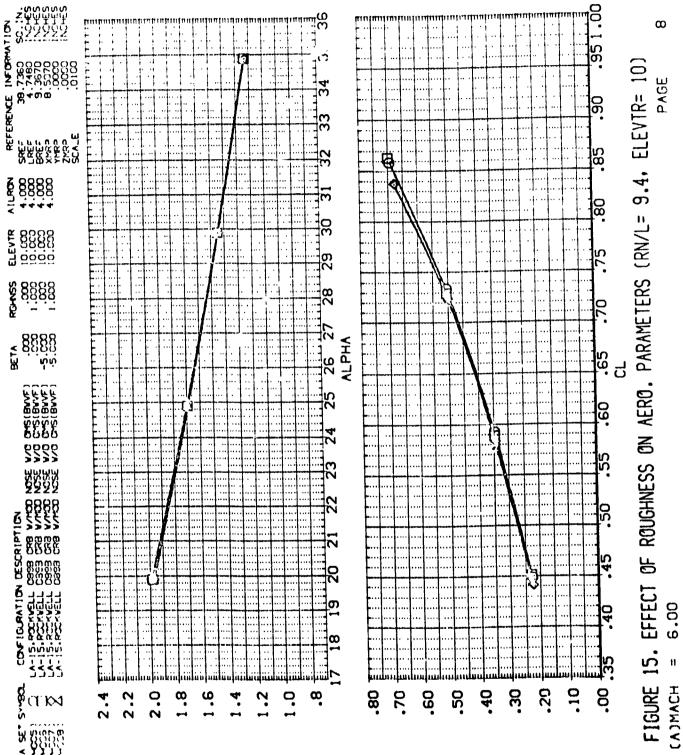


OF ROUGHNESS ON AERO. PARAMETERS (RN/L= 9.4, ELEVIR= -5) EFFECT 6.00 FIGURE 14. (A)MACH





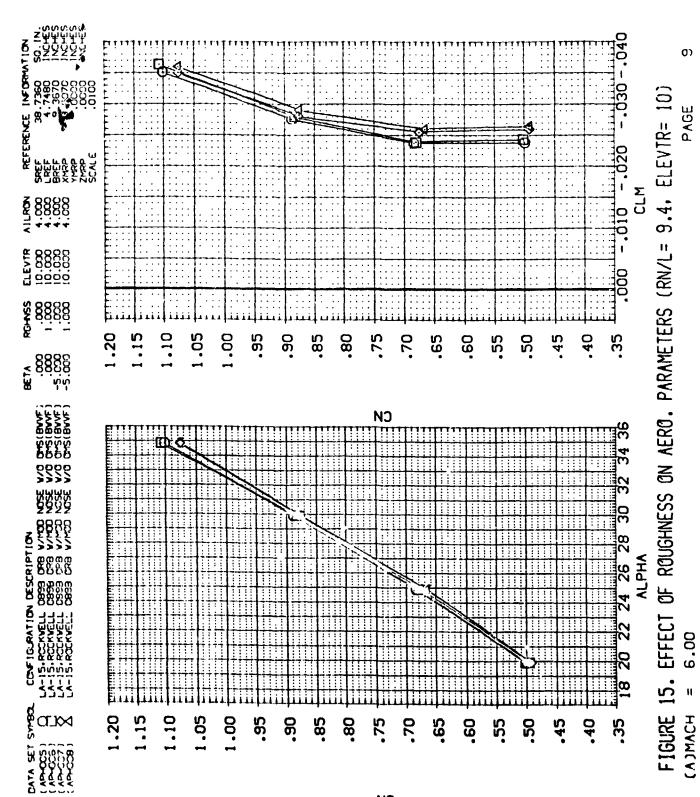




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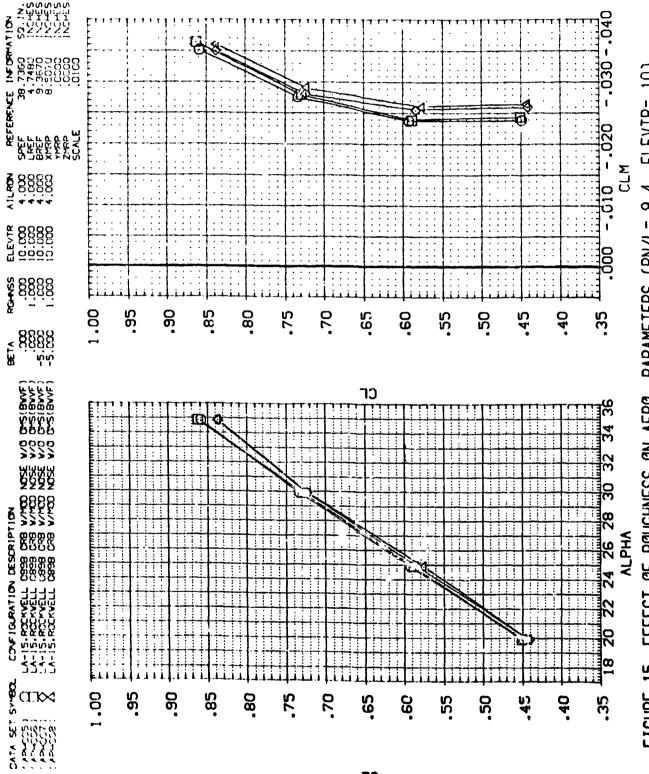
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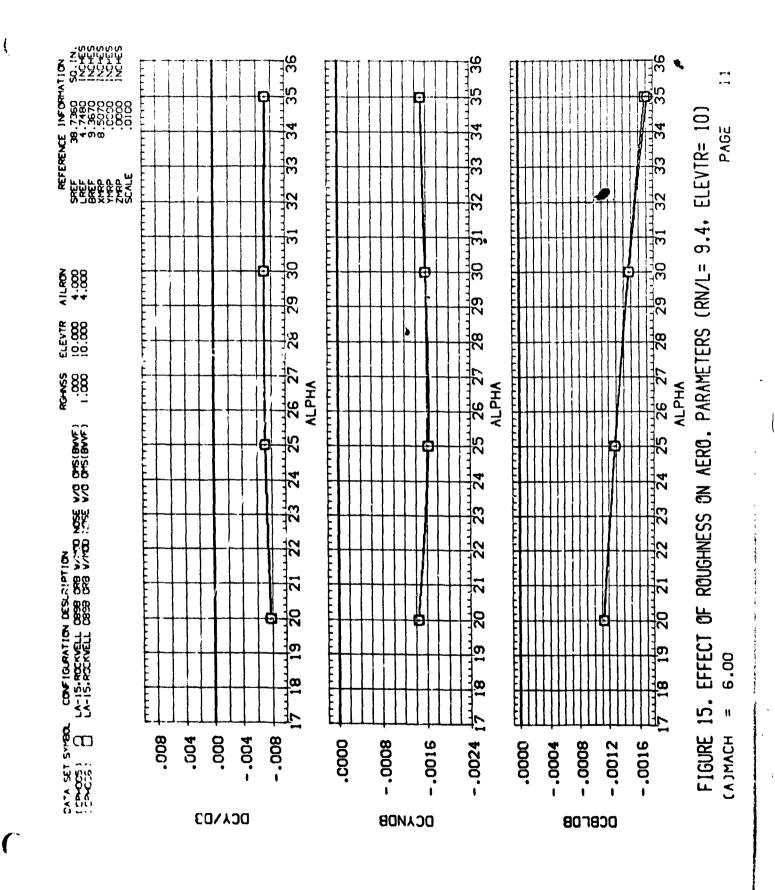
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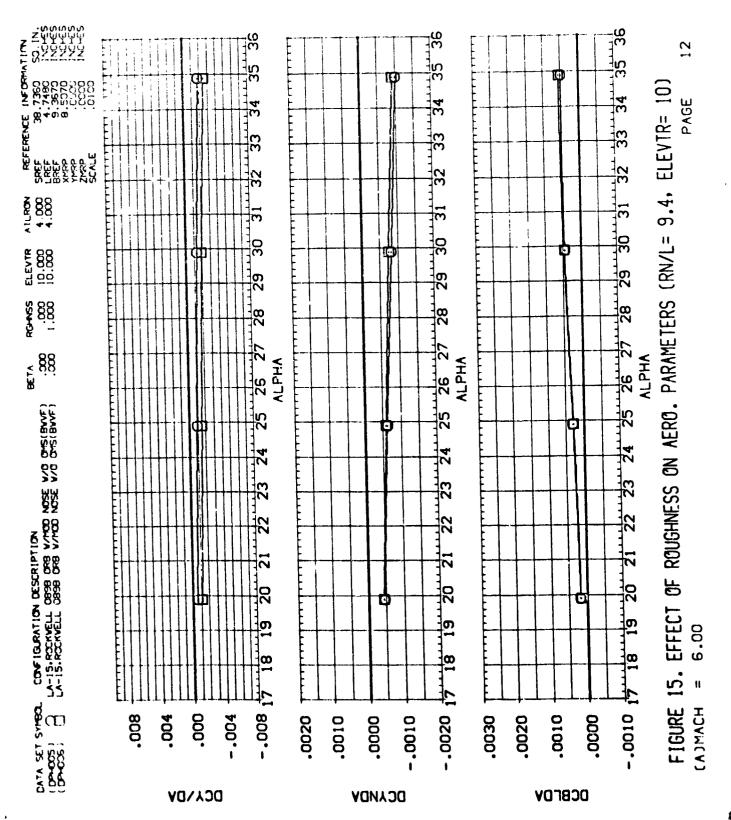
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EFFECT OF ROUGHNESS ON AERO. PARAMETERS (RN/L= 9.4, ELEVTR= 10) 6.00 FIGURE 15. I





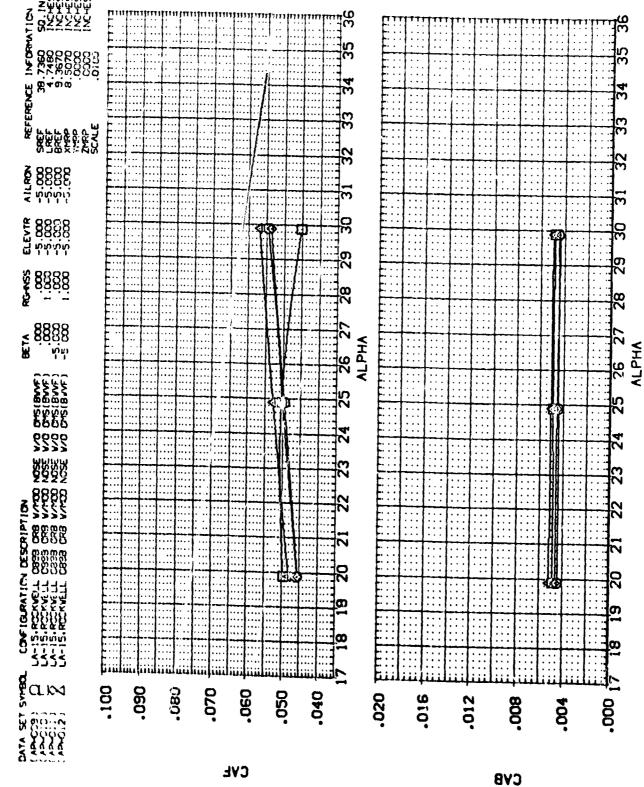
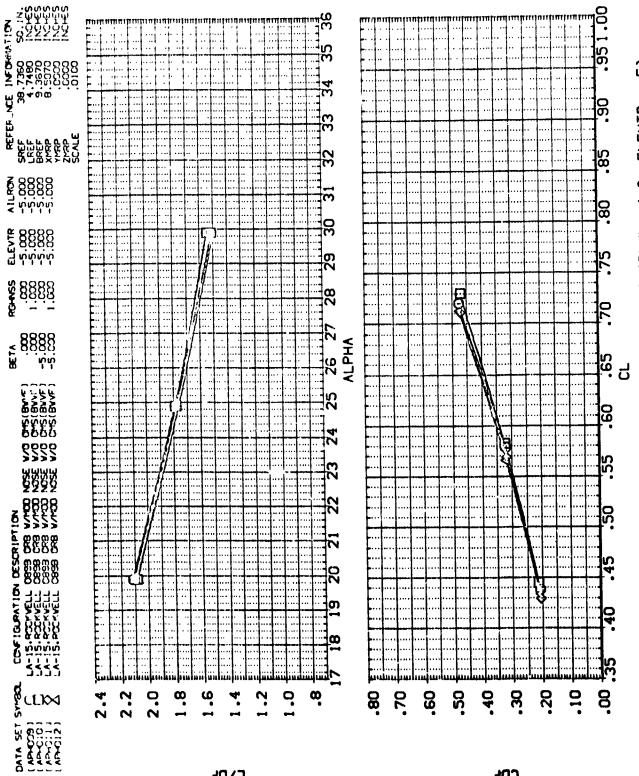


FIGURE 16. EFFECT OF ROUGHNESS ON AERO. PARAMETERS (RN/L= 4.0, ELEVTR= -5) 5.93 CA JMACH

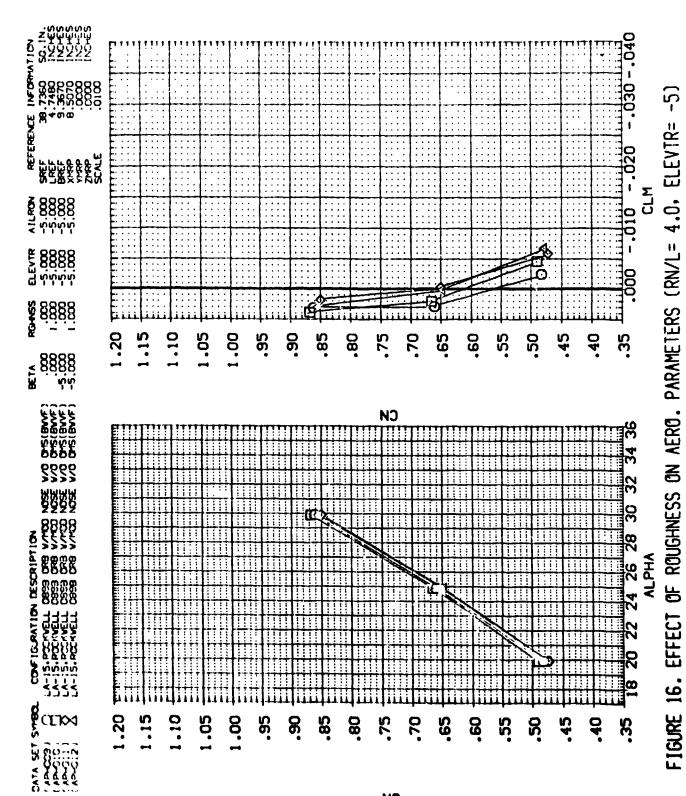


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FIGURE 16. EFFECT OF ROUGHNESS ON AERO. PARAMETERS (RN/L= 4.0, ELEVIR= -5) 5.93 CA JMACH

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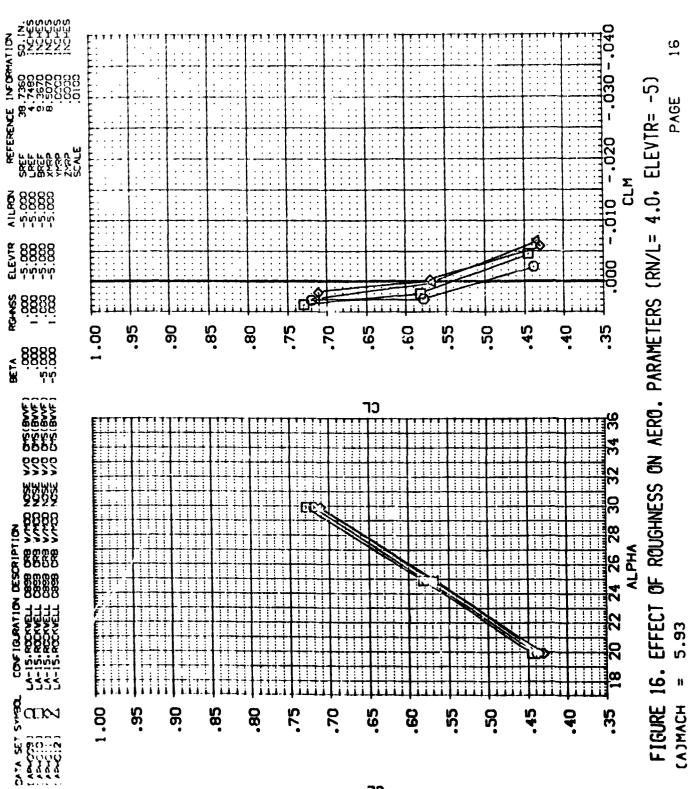


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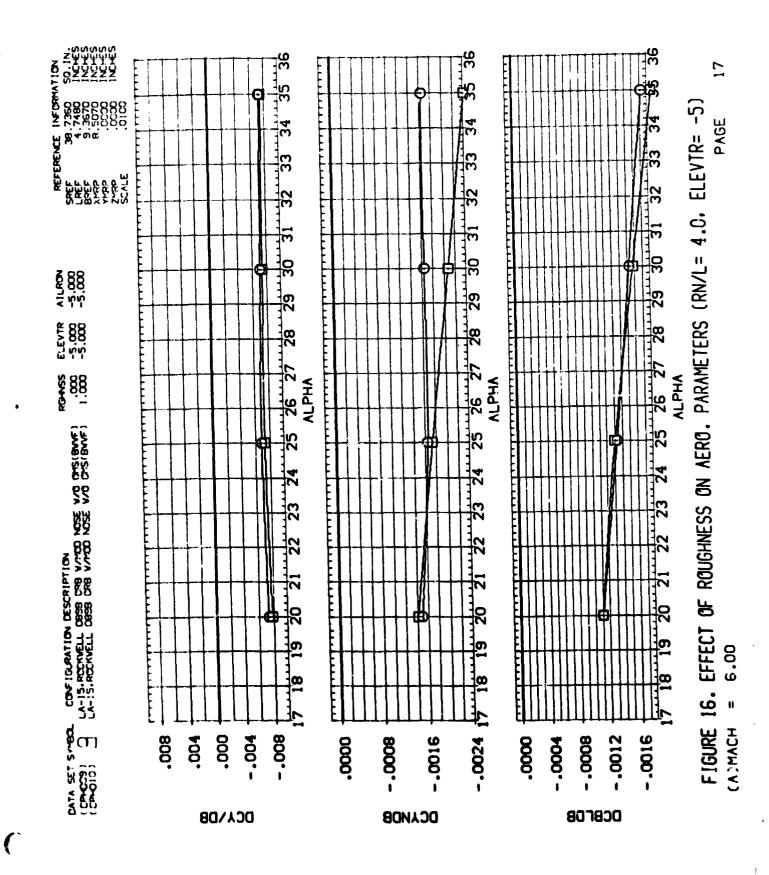
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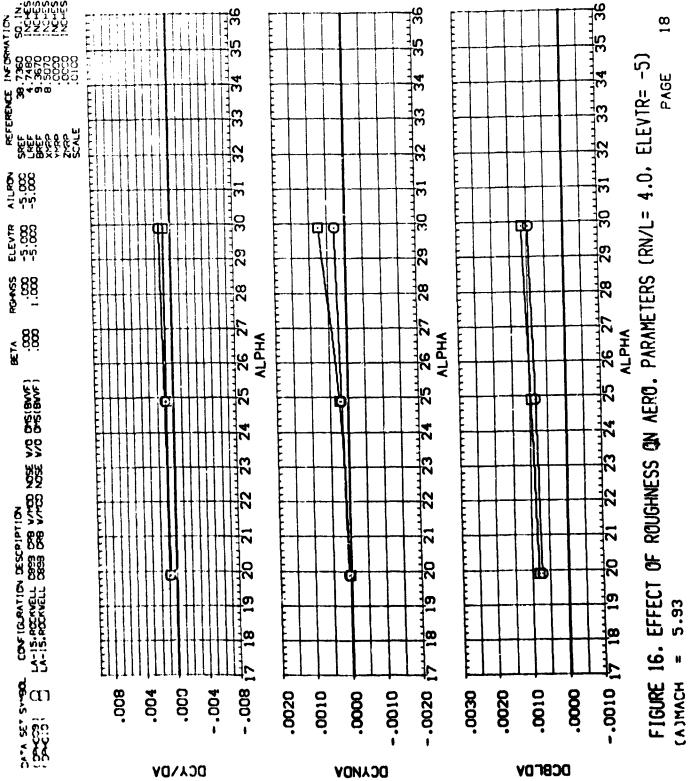
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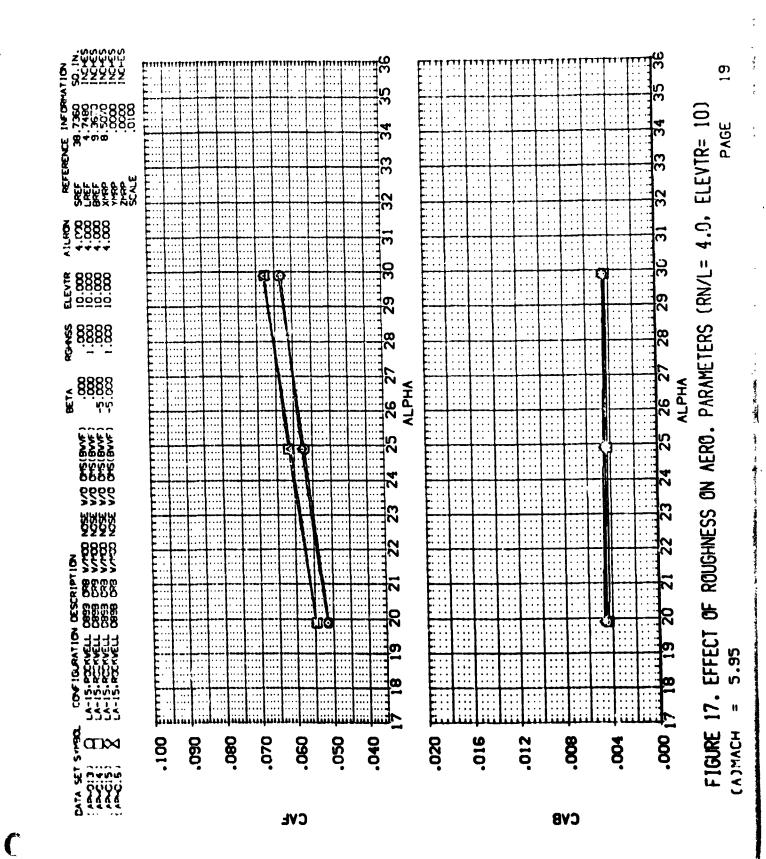
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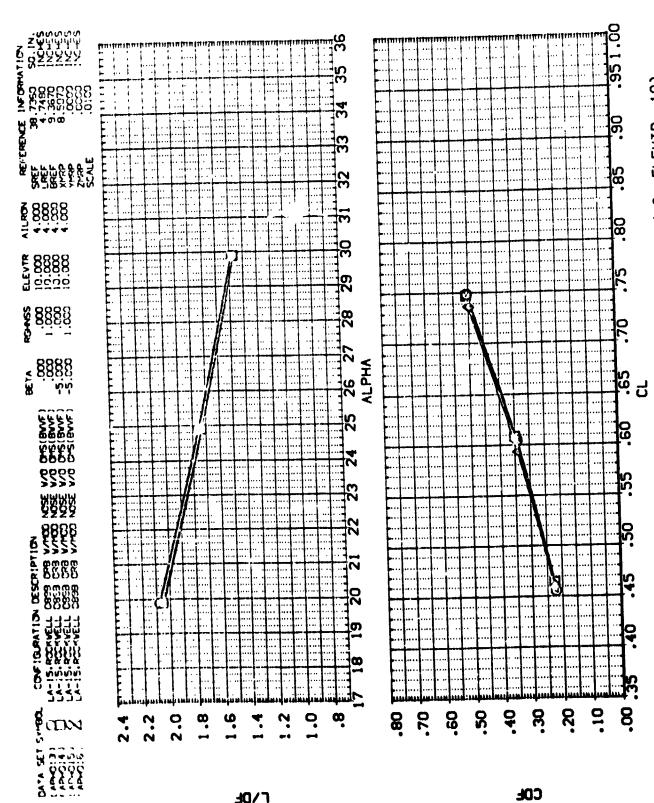
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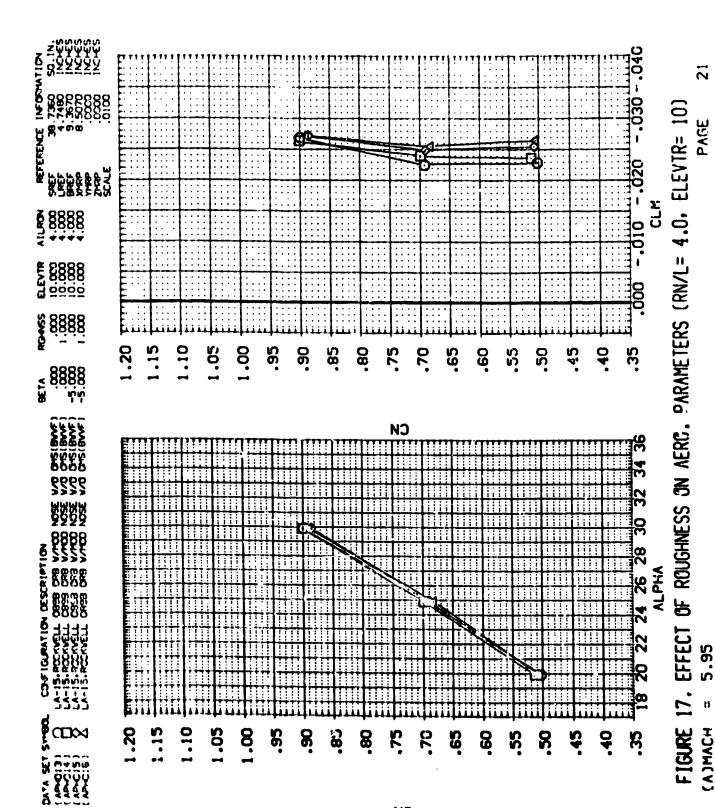


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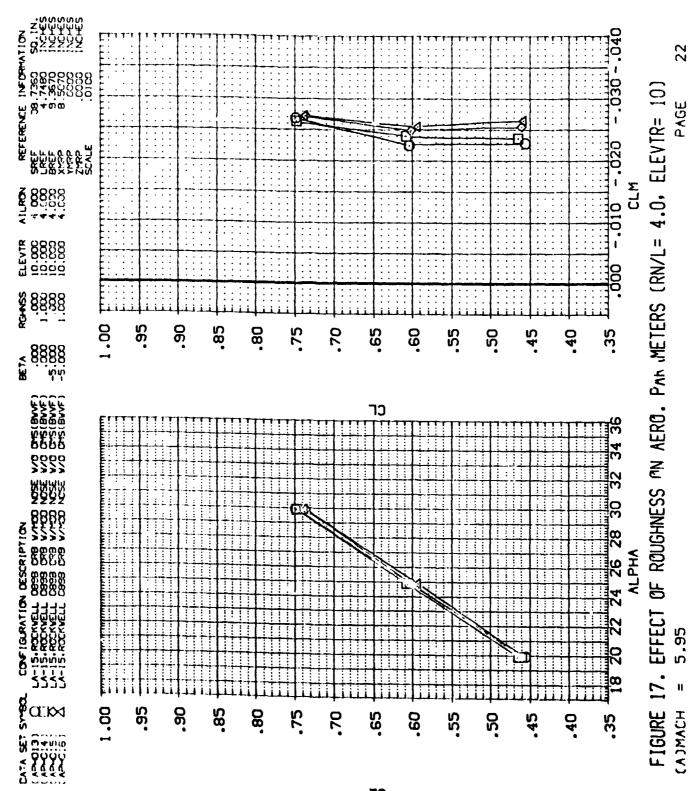
20 FIGURE 17. EFFECT OF ROUGHNESS ON AERO. PARAMETERS (RN/L= 4.0, ELEVTR= 10)
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(A)MACH = 5.95

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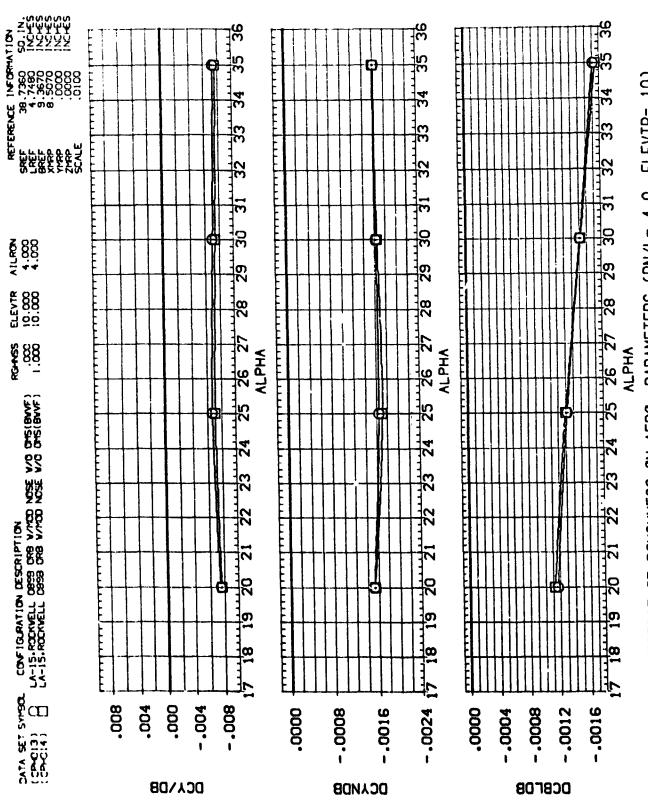
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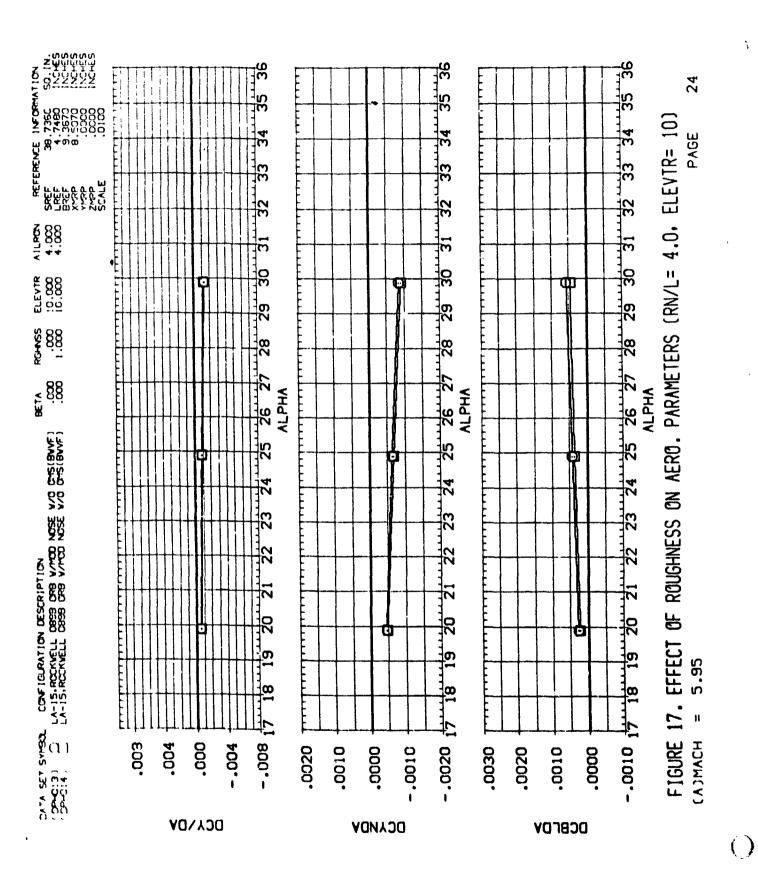
FIGURE 17. EFFECT OF ROUGHNESS ON AERO. PARAMETERS (RN/L= 4.0, ELEVTR= 10)

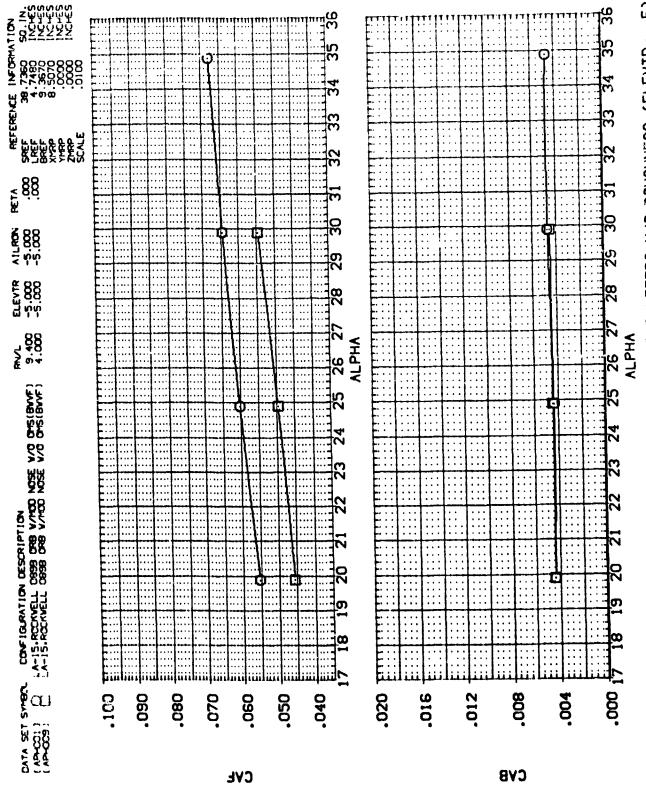
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FIGURE 18. EFFECT OF REYNOLDS NO. ON AERO. PARAMETERS W/O ROUGHNESS (ELEVTR= -5) CAJMACH

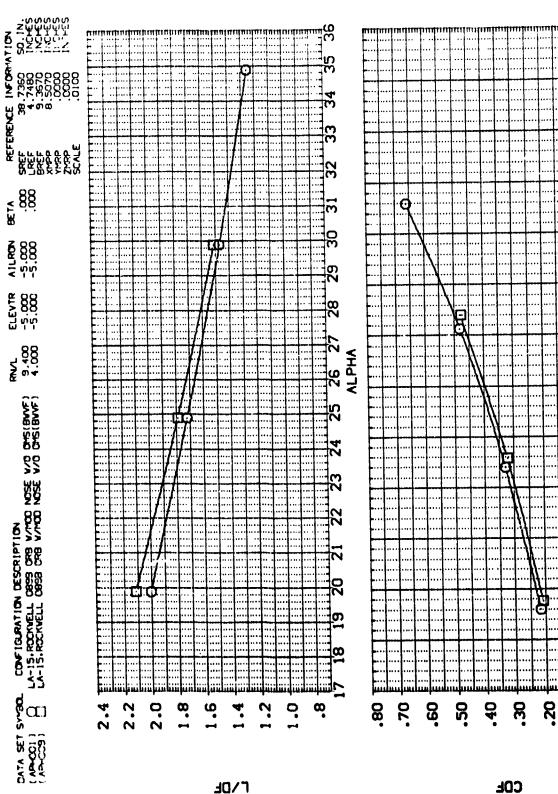


FIGURE 18. EFFECT OF REYNOLDS NO. ON AERO. PARAMETERS W/O ROUGHNESS (ELEVTR= -5) (A)MACH

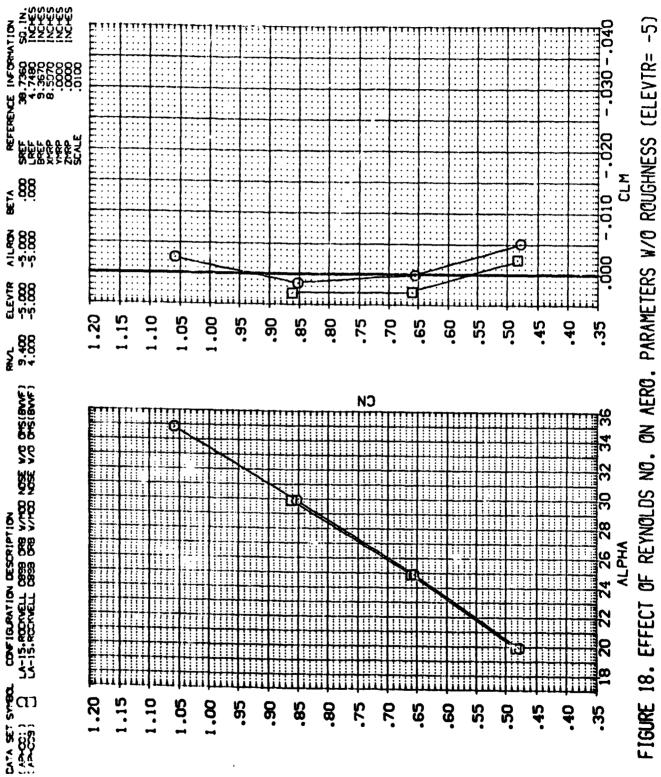
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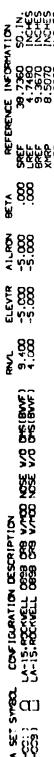
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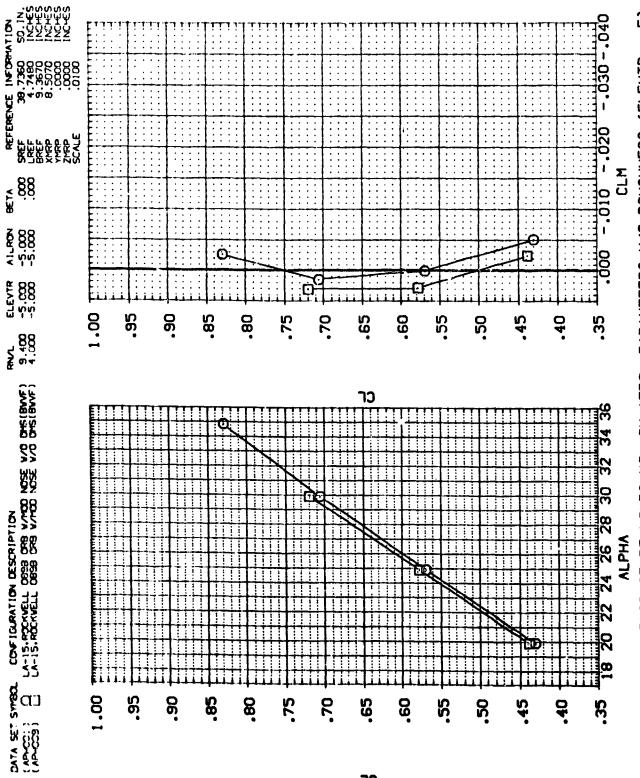
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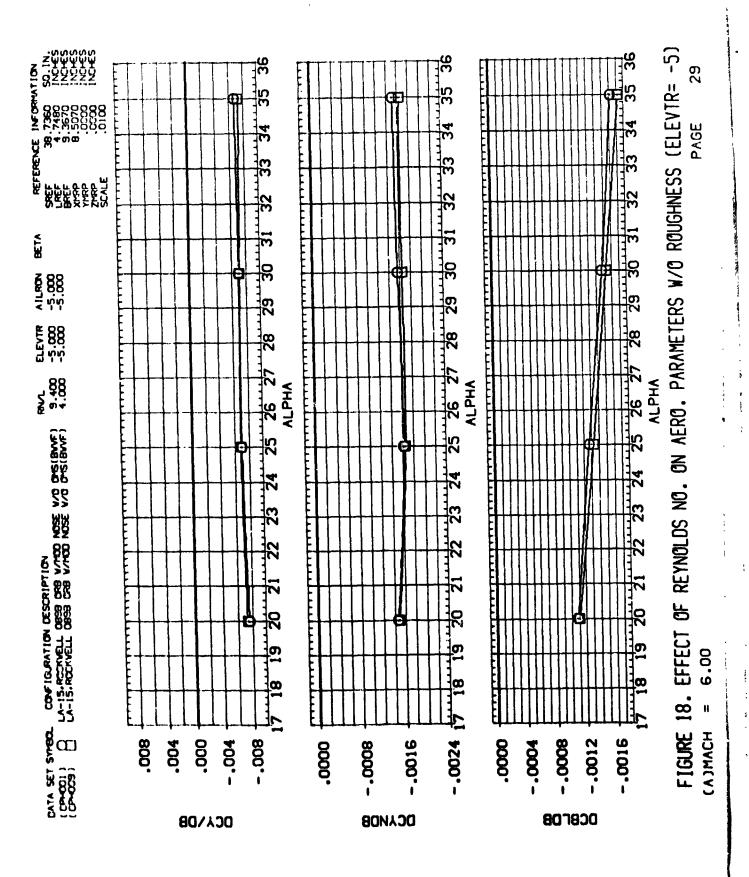
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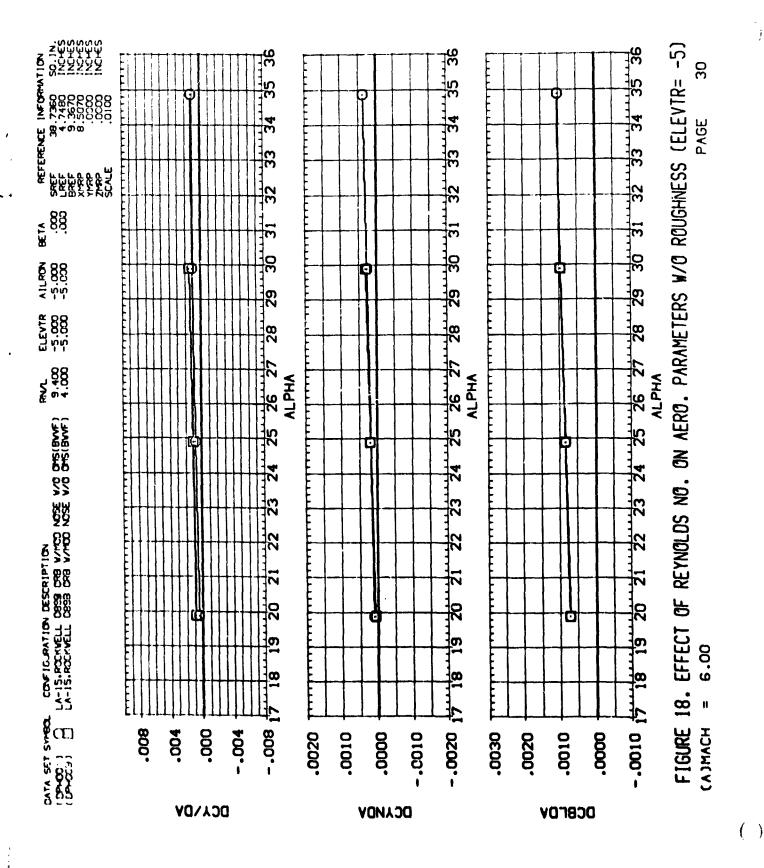


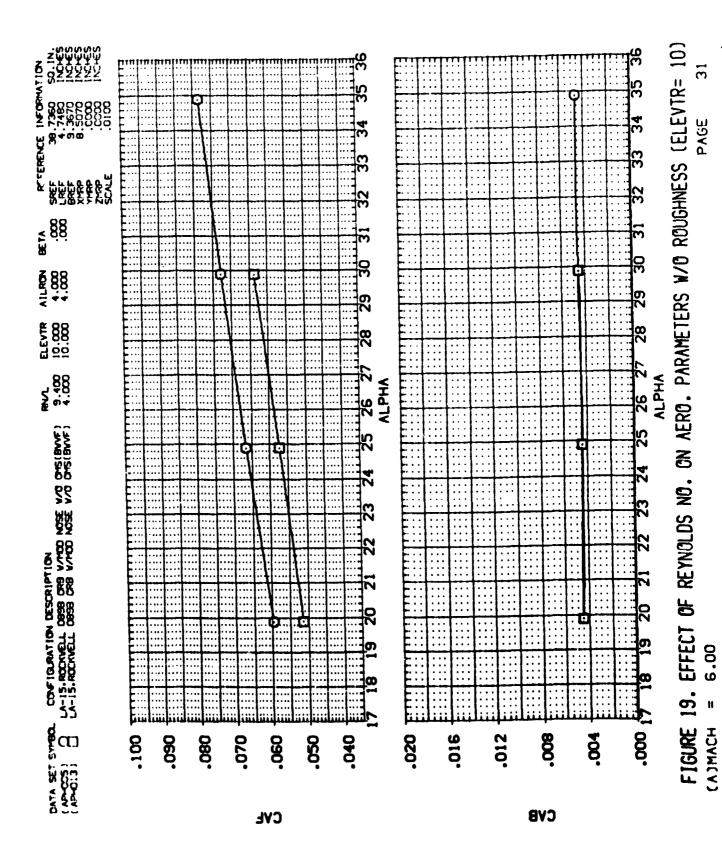
EFFECT OF REYNOLDS NO. ON AERO. PARAMETERS W/O ROUGHNESS (ELEVTR= -5) 6.00 6.00 18. FIGURE (A)MACH

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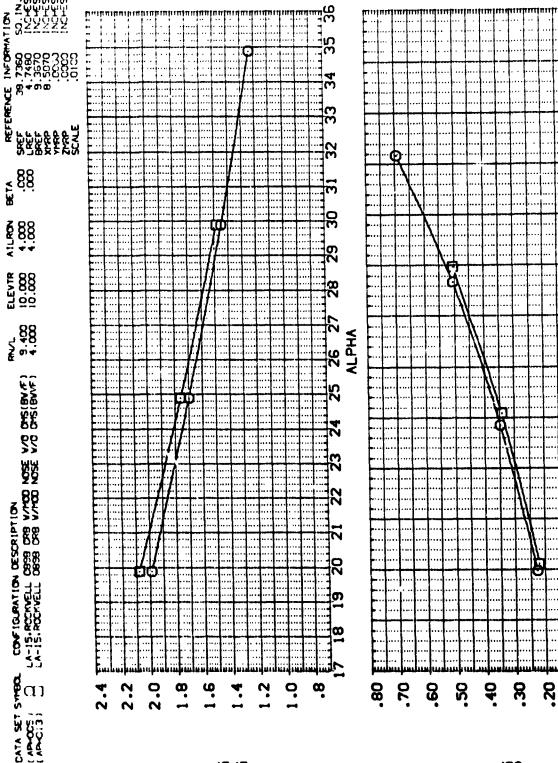


FIGURE 19. EFFECT OF REYNOLDS NO. ON AERO. PARAMETERS W/O ROUGHNESS (ELEVTR= 10)

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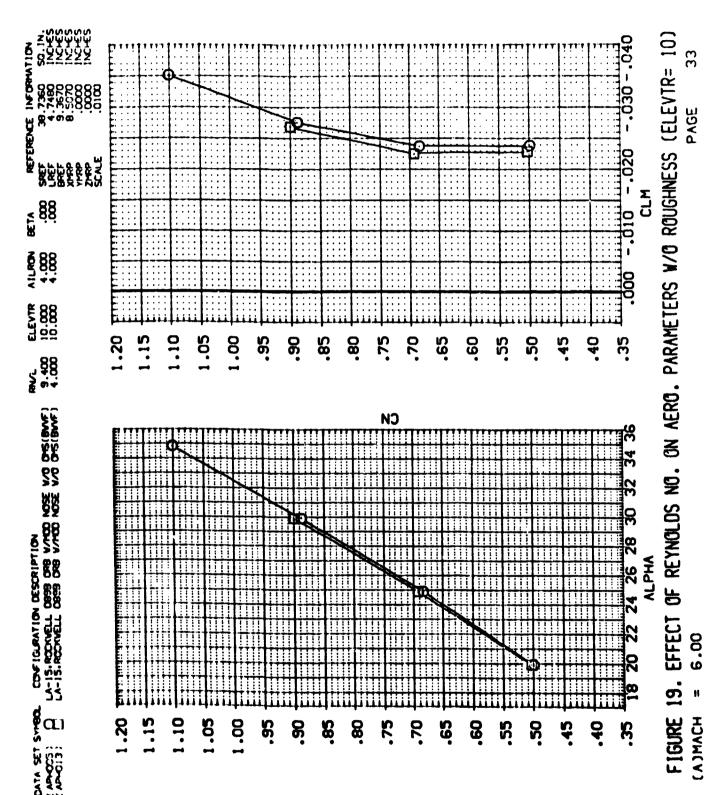
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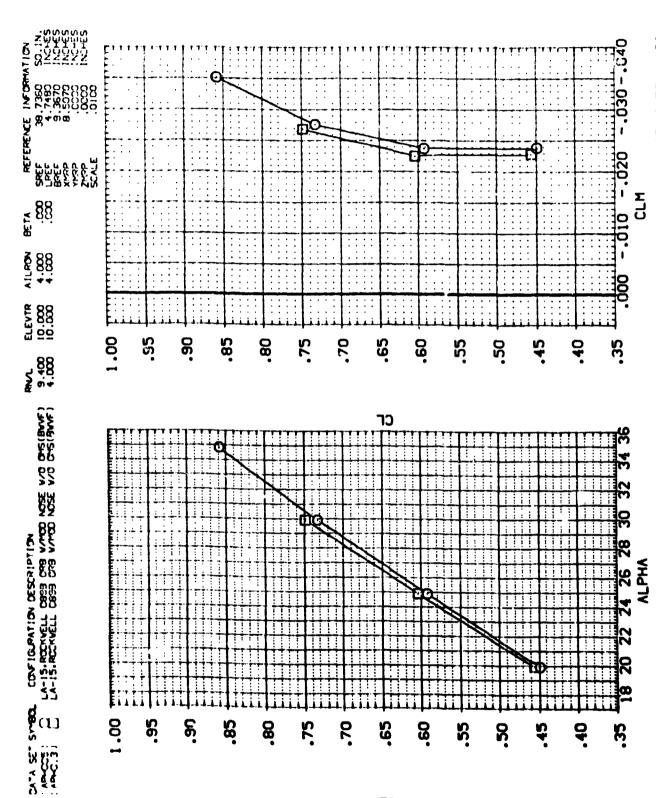
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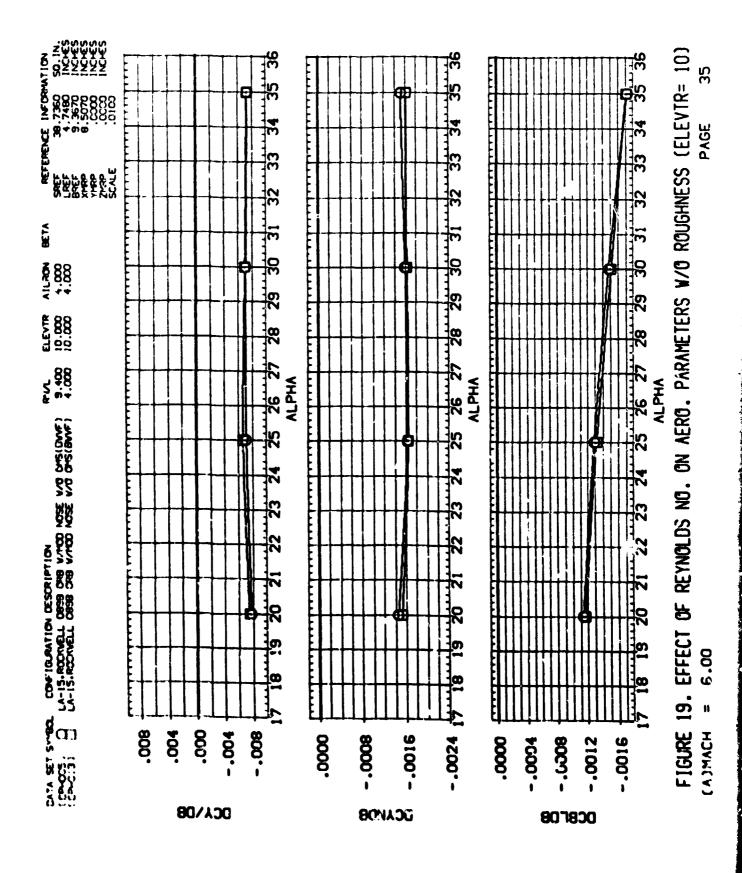


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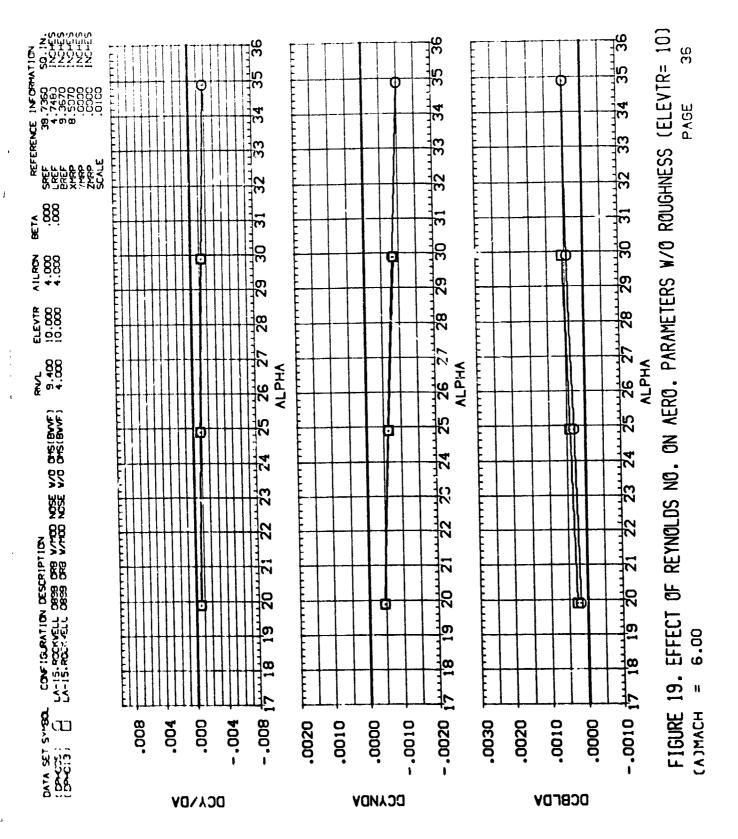


EFFECT OF REYNOLDS NO. ON AERO. PARAMETERS W/O ROUGHNESS (ELEVTR= 10) 6.00 FIGURE 19. CA JMACH

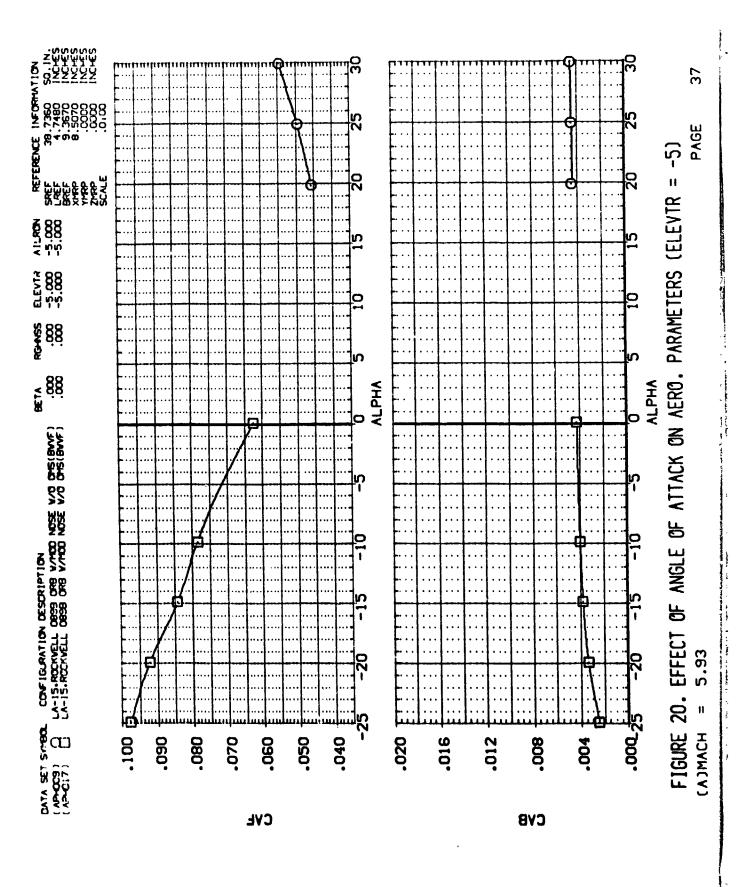
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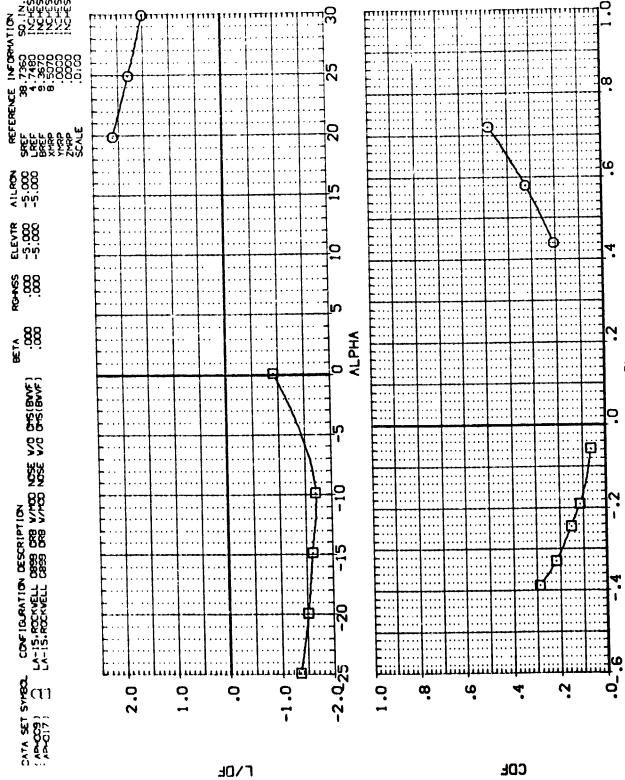
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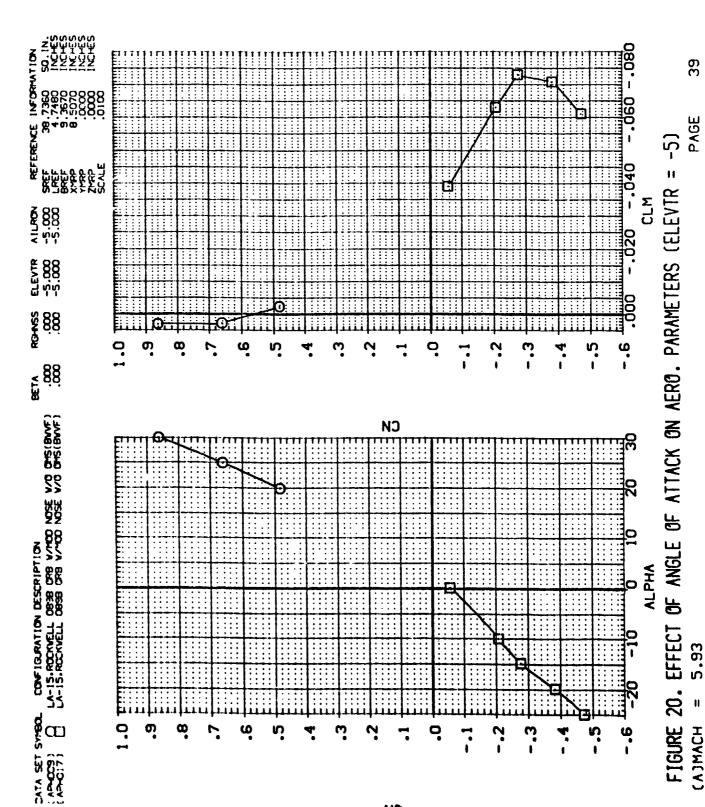
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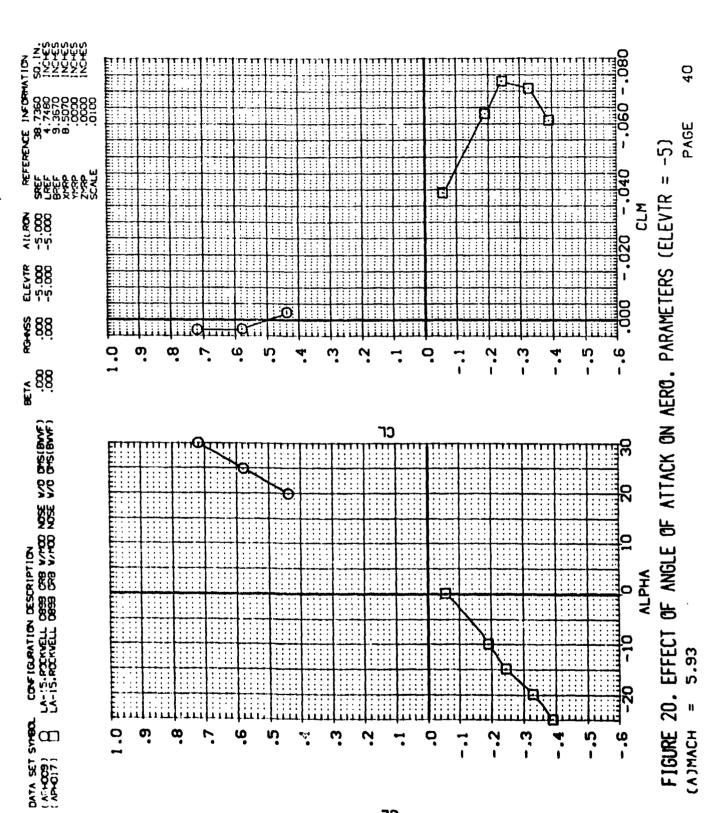


PAGE FIGURE 20. EFFECT OF ANGLE OF ATTACK ON AERO. PARAMETERS (ELEVTR = -5)

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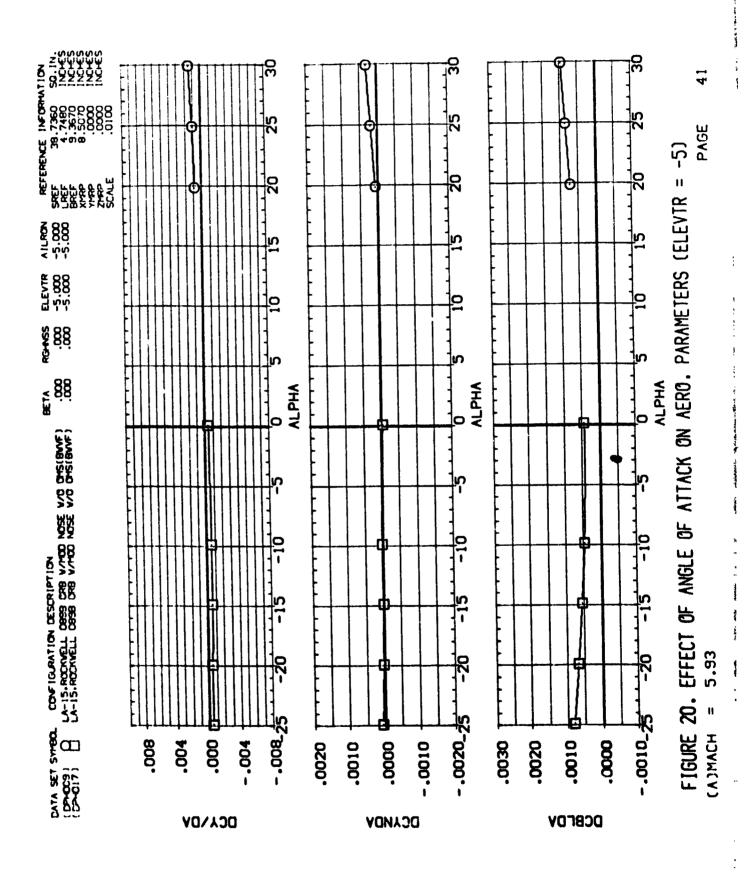
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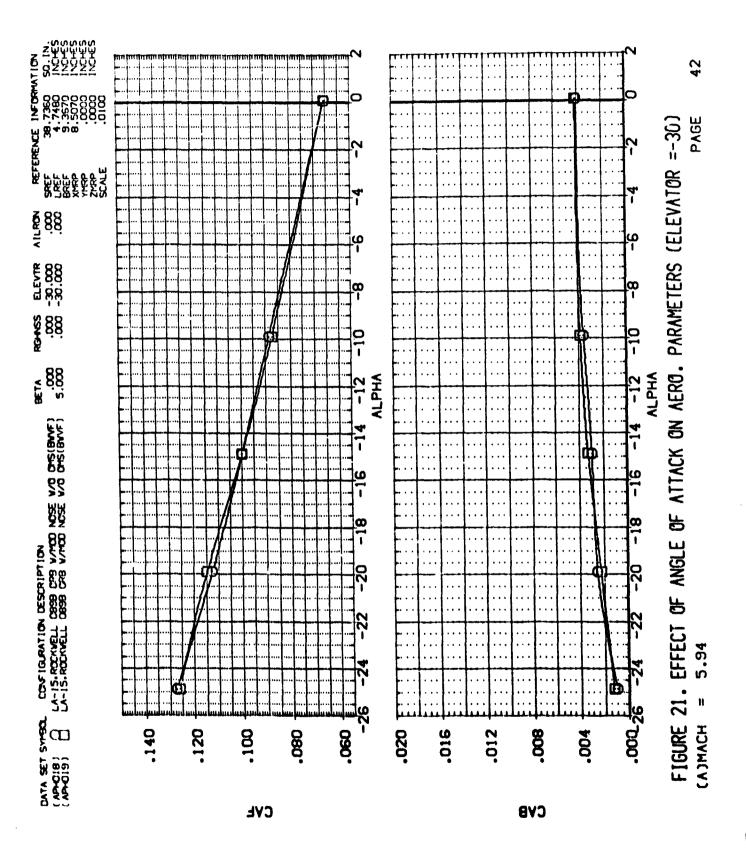
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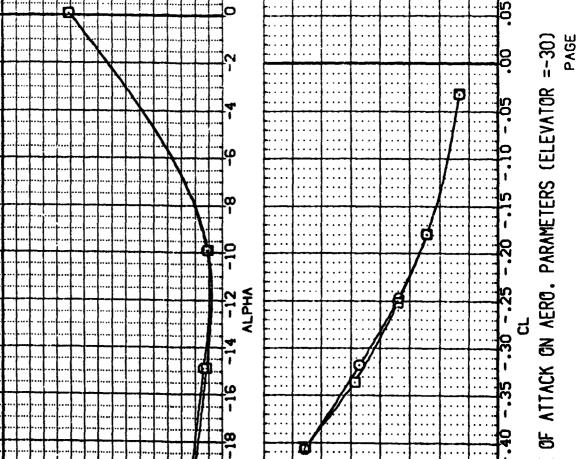


FIGURE 21. EFFECT OF ANGLE OF ATTACK ON AERO. PARAMETERS (ELEVATOR =-30) (A)MACH

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COSTIGARATION DESCRIPTION

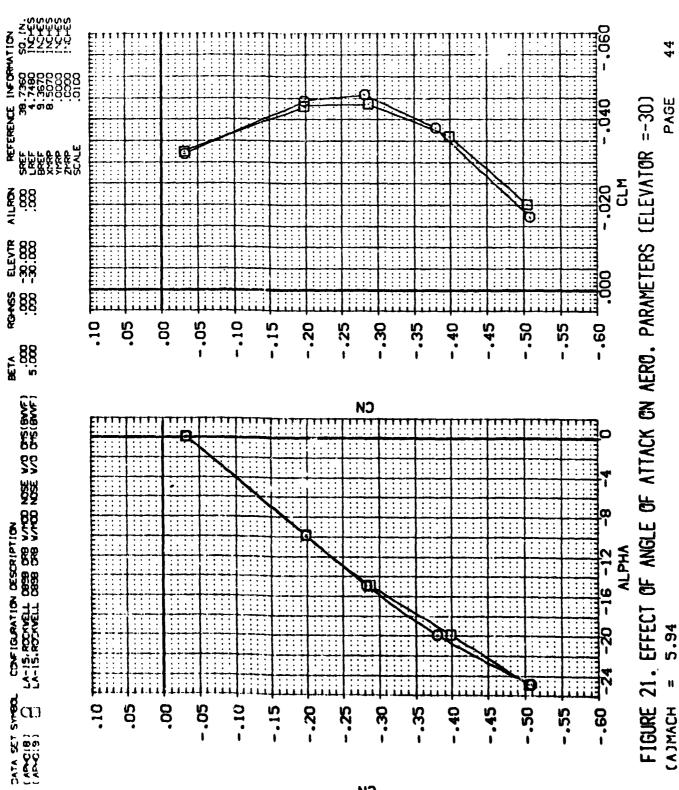
LA-15, ROCKVELL 0898 CR8 V/MOD NOSE V/O OFS(BNYF)

LA-15, ROCKVELL 0898 OR8 V/MOD NOSE V/O OFS(BNYF)

CAPACIES CAPACION CONTROL CAPACION CAPACION CONTROL CAPACION CAP

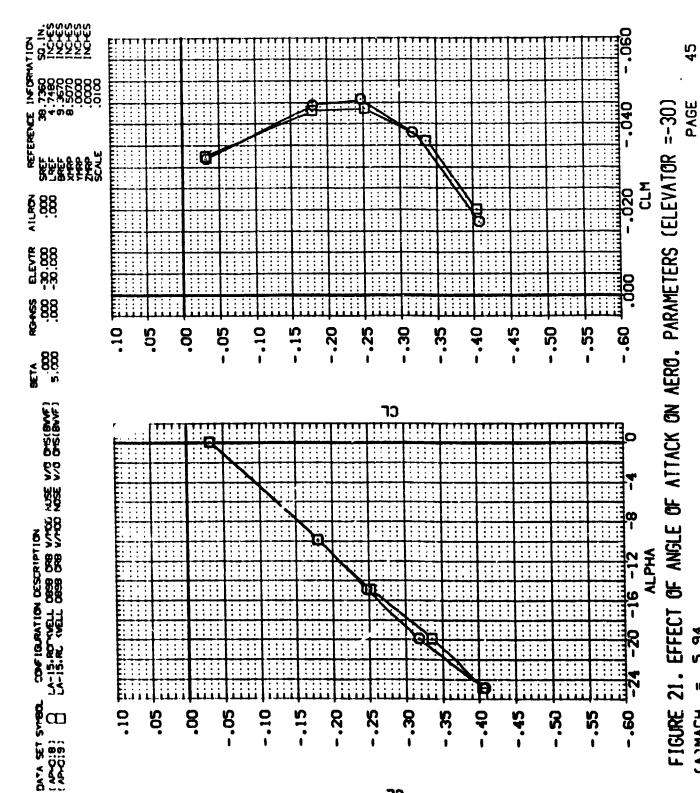
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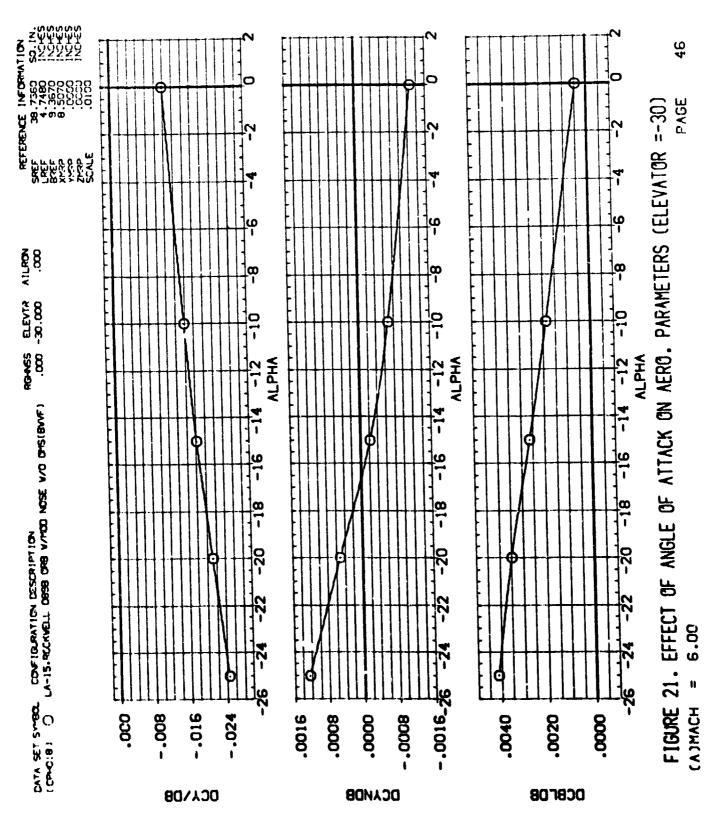
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APPENDIX

TABULATED SOURCE DATA

Plotted data are available from the DMS on request.

TABLATTO SOURCE DATA, LAKE TO INCH HE-4441, (LA-15) SEE : 8.5077 INDES WETA

1	1			TABULATED SO	TABULATED SOURCE CATA, LARC 20 INCH HE-6441, (LA-15)	LARC 20 1M	CH HE-6461,	(LA-15)				PAGE 2	
	! !			LA-19,62CM	LA-19, POCRUELL DOPR ORB WAND NOSE W/O CHS (BANF)	WHOS NO	SE W/O CHS (F	3796)		(RPHENDS)		(10 JAN 74)	
		AVA TOTAL	•						PARA	PARAMETRIC DATA	DATA		
	36.7360	. is		23-C341 040-2-6 23-C341 0000	5 5 C			BETA ATLRON	, , , , , , , , , , , , , , , , , , ,		ELEVTA :	000.8-	
 Kore		S C		SOON THOUS	5					. 400			
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	•		-5.00000 -5.00000	6,12962 6,08661 -,00016	2.00.1 0.00.1 0.00.1	S 2000		00000	.00982	.02000. 00050	•	00000	
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			9	0 /\$	BA = 0.80	GRADIÐA	GRADIENT INTERVAL =	-5.00/	8.8				
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DATE 21 JAN 74			TABULATED SOURCE DATA, LARC 20 INCH HE-6441, (LA-15)	URCE DATA,	LARC 20 IN	CH HE-6441,	(LA-15)			•	PAGE 3	
			1.A-15,ROCK	אברר מפשפ ספ	ON OUM/M BE	A-15, ROCKHELL D896 ORB WAND NOSE W/O OMS (BANF)	BANE)		(RPHOOS)		(10 JAN 74	_
	REFERENCE DATA	۶						PAR	PARAMETRIC DATA	DATA		
9407 : 36. UBC : 4. SCAE : 9.	98.7360 98.1N. 4.7480 INDES 9.3670 INDES	11 11 11 11 11 11 11 11 11 11 11 11 11	6,9070 INCHES ,0000 INCHES ,0000 INCHES	3 5 5 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5			BETA AILRON RUDFLR RN/L	8 H II B	.000.	ELEVTR = RUDGER = RGMNSS =	10,000 ,000 ,000	9 5 5
		EN NO.	59/ 0 FBV	FRIAL = 8.80	CRADIENT	GRADIENT INTERVAL =	-5.00/ 5	9.00				
. me . me 	A.P.M. 19.000 24.000 25.000 34.000	META .00000 .00000 .00000 .00000	4 (PSI) 6.18932 6.18157 6.25438 6.25471	.49803 .49803 .66403 .101109 .101021	CAF .05966 .06559 .07274 .00125	ALM 02363- 02732- 02732 03073	CBL .00073 .00123 .00160 .00195	CYN -,00173 -,00247 -,00327 -,00403 -,00015	CY -, 00210 -, 00351 -, 00524 -, 00730 -, 00005		CAB .00446 .00486 .00461 .00466	
		į	LA-15,ROCK	0 8690 TIPO	RB WASO K	LA-15,NOCIULELL DESE ORB WATCO NOSE WO ONS (BLAF)	(BuMF)	A	(RPHODS) PARAMETRIC DATA	5) (10 DATA	(10 JAN 74	_
	96,7360 80.1N. 4,7460 1NOES 9,3670 1NOES ,0100	7.V	63-041 0000. 63-041 0000. 63-041 0000.	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5			BETA ATLRON RUDFLR RWAL	# H H H	.000 .000 .000	ELEVTR = RUDJER = RGHNSS =	ŭ ,	000*
		RUN NO.	53/ O RPC	RV. = 8.75		GRADIENT INTERVAL =	-5.00/	8.8				
2 8 8 F	24.290 24.290 25.290 26.290 34.280	20000 20000 20000 20000 20000	6.23402 6.18649 6.23730 6.36008	ON . 50102 . 68013 . 86297 1.10731	.06064 .06709 .07313 .07934	0000	.00119 .00190 .00224 .000011	CYN -,00172 -,00235 -,00369 -,00013	-,00452 -,00452 -,00603 -,00764		CAB .00447 .00437 .00467 .00470	

			TABULATED S	TABULATED SOURCE DATA,	LARC 20 19	LARC 20 INCH HE-6441, (LA-15)	(LA-15)			PAGE 4
DAIL CI JAN T			LA-15,ROC	LA-15, ROCKHELL 1898 ORB W/MOD NOSE W/O CMS (BAMF)	RB W/MOD NK	SE WO CHS	(BLAYF)		(RPHOOT) ((10 JAN 74)
		;						PARA	PARAMETRIC DATA	
	reference on	Į.								1000
- 199.	38,7360 SQ. IN.	XP#RP ==	8,5070 INCHES	NCHES			BETA ATI BON	, 81 81	-5.000 ELEVIN	. 11
н		YMRP =	. DODD INCHES	MCHES				. 11		000.
11	9.3675 INCHES	ZMRP =	. DODD INCHES	NCHES			RNA	"		
# ***										
		RUN NO.	60/ D RN	RN/L = 6.86	GRADIENT	GRADIENT INTERVAL =	-5.00/	9.00		
				i	į	3	é	CAN	Շ	CAB
MACH	*	BETA	a (PST)	5		10464	96300	.03543	.03673	.00460
110.0		-5,00000	6,12301	.49107	Tage .	97570	.00763	.00563	00250.	.00460
600.0		-9.00000	8.14535	67419	C1000.	02611	\$1600.	0,000	.03030	.00459
6,004	29.69	-5,00000	8.10727	*******	57845	-,03489	.01055	.00354	.02915	.00449
•.003	SACIENT		.00237	616EU.	.00121	-, e2005	.00028	-,00013	-,00049	-,00001
			LA-15,ROC	LA-15, ROCKLETL (1898 ORB W/WOD NOSE W/O CHS (BAMF)	N OCHAM SEK	DSE N/O CHS	(Buvf)		(RPHODB)	10 JAN 14)
								PARA	PARAMETRIC DATA	
	REFERENCE DATA	TA T							·	
		995	A. SOZO INCHES	INCHES			BETA	1		
P3 H1	36,7360 Se. IN.		DOND INCHES	NOES			AILRON	6	4.000 RUDDER	
n H			CODO INCIES	INCIES			RUGUE A	H H	. 000.	ı
								1		
		RUN NO.	SA 0 /28	RN/L = 8.86		GRADIENT INTERVAL =	-5.00/	3.00		
		į	0/6671	č	3	ē	e	3	Շ	C.B.
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6.00°	19.09	-5.00000	6,16955	.66576	.06697	02594	.00756	.00581	58620	.00459
970.9	200	-5.00000	0.19762	.6757	.07352	50620*-	12600.	66700	.02771	9700
- GOD	74,090	-5,00000	8,22634	1.07594	.07897	06550	79010.	1000	09000-	10000
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5.935		coord.	20770	. 86195	.05454	.00304	-, 99480	-,00152		.00451
5.937	060.62	OCCUPANT.	06000	.03792	69000	.00054	00012	-,00012	00030	. Othor
	CRADIENT	· Partiral	•							

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מאוב כז זשה כ	•		LA-15,800	LA-19, ROCKHELL DOOD OND W/NOD NOSE W/O CHS (BANF)	ORB W/NOD IX	DSE W/O OMS	(Buvr)		(RPH010) ((10 JAN 74 J	
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1 .6		00000	3.49016	.66510	.09041		- 00577	-,00376	-,00434	007499	
5.933	5	00000	3.50531 D0444	.08747	00043	79000	71000	-,00036	-,00001	00000	
			CA-15.RO	LA-15,ROCYLELL DOOR ONE W/O ONS (BAMF)	ORB W/HOD N	DEF W/O CHE	(BANE)		(RPH011)	(10 JAN 74)	
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Ŏ.		DETA		7 A 7 A 7 A 7 A 7 A 7 A 7 A 7 A 7 A 7 A	.04552	-,00584	.00186	01200.	.03255	. 00459	
9.93		-5.00000	3.47610	65026	,0900A	-,00027	.00240	.00731	.02665	.00439	
8.838		4-	3.40064	.65048	.05370	.00101	.00281	99900	06730.	e de la constant de l	
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	ADPENDICE DATA	\TA						ž	PARAMETRIC DAIA		
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	36.7360 58.IN.		0.5070	6.5070 INCHES			אַל	11 Z	-5.000 RUDDER	n	
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9.94		-9.0000	3.4079	A2750	70750	06200	60200	.00655		.00500	
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\$\$ \$24.900 .00000 .000000 .000000 .000000 .000000 .000000 .000000 .000000 .000000 .000000 .000000 .000000 .000000 .000000 .000000 .00000	8.93				40204	.05736	02250	.00165	00253	UND 42		. ,
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Section Sect				LA-15,800	DOMENT DISSES	RB W/NCD N	EDGE M/O CHES	(BrAF)				
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## 39.790 34.1N, 949			1									1
Section Set, 114, 1969				1				VT.30	*		11	10,000
## 9.3870 INCRES 294F = .0000 INCRES RUPL = 3.67 GRADIDMT INTERVAL = -5.007 \$.000 RCHMSS = 3.1		36.7360 SQ.IN.		8.30V	INCRES			AIU				000
## 9.3870 INCRES 2969 =0000 INCRES ###O1 ALPNA EETA 84731 ON CAF CAB COURS		4.7480 INCHES		oraco.	INCHES			RUDA				1,000
### 10100 MACH MACH EETA 0-8710 CN CAF CLN CBL CTN CT CAB		9.3670 INDES		0000	INCHES			25	ħ	4,000		
RAM NO. 57 0 RW/L = 3.67 GRADIBMT INTERVAL = -5.00/ 5.00 MAPPER	CALE =	,0100										
##CHAIN BETA 64951) CN CAF CLH CBL CYN CY CAB \$1.55.55 19.5800 3.54143 6.98644 0.05470 -0.02392 0.00099 -0.00169 -0.00000 0.00429 \$1.59.55 29.5800 0.02374 3.69374 0.05470 -0.02397 0.00142 -0.00249 -0.00209 \$1.59.55 29.5800 0.02374 3.69374 3.00379 0.00379 0.00009 -0.00149 -0.00299 0.00429 \$1.59.55 29.5800 0.02374 3.00379 0.00379 0.00009 -0.00149 -0.00299 0.00000 \$1.59.55 29.5800 0.02374 3.00379 0.00379 0.00009 -0.00149 -0.00299 0.00000 \$1.59.55 29.5800 0.02374 3.00379 0.00009 0.00009 -0.00149 0.00009 0.00009 \$1.59.55 29.5800 0.02374 3.00374 0.00009 0.00009 0.00009 0.00009 \$1.50.50 0.0000 0.0000 0.0000 0.00009 0.00009 0.00009 0.00009 0.00009 \$1.50.50 0.0000 0.00000 0.00009 0.00009 0.00000 0.00009 0.00009 \$1.50.50 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 \$1.50.50 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 \$1.50.50 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 \$1.50.50 0.000000			RUN ND.					-5.00/	8.			
##CHANNEL NOTION 3-19471				i	i	4	3	ŧ	£	Շ		
\$1.950 24.450 .00000 3.54143 .6964 .00170 .00142 .00	OW		DETA	0.5313	5		- 02352	69000	-,00189	-,00200		-
\$.599	ě, n		00000	3.56703	08116.		1910	.00142	00274			S.
### ##################################	6.0		goode.	3,54143	10000	0.100	5000	06100	00367			Ņ
### 39.770 NOSE W/NTO NOSE W/O CHS (BANF) (RPHD15) (1D JAN 7) ###################################	e e	2	como.	5,49374	.03576	06100	-,00026	60000	-,00014			g
### 39.7360 59.1N. 1966 = 0.5070 1NG-ES = 39.7360 59.1N. 1966 = 0.5070 1NG-ES = 4.7460 1NG-ES				00.51-4-	0690 TUPOU	CHE WATC	NOSE W/O OM	S (BLAVE)		(RFH015)	AL 01)	2 2
# 30,730 50.1N. Note = 0.5070 INCHES # 4,7400 INCHES				<u> </u>					9	SAMETRIC DA	4	
# 39.7340 39.114. Name = 6.5070 INCHES # 4.7460 INCHES = 10000 INCHES # 4.7460 INCHES = 10000 INCHES = 100000 INCHES = 10000 INCHES = 100000 INCHES = 1000000 INCHES = 100000 INCHES = 100000 INCHES = 100000 INCHES = 1000000 INCHES = 100000 INCHES INCHES INCHES INCHES INCHES INCHES INCHES INCHES INCHES = 100000 INCHES IN			1TA						2			
# 39.7340 39.114, 3988 # 8.5070 INCLES # 4.7440 INCLES									11			10,000
# 4.7460 [VOCES VMPP = .0000 [NOCES RUOTLE = .000 ROHNSS = RUOTLE = .000 ROHNS = RUOTLE = .000 ROHNS = .000		36.7360 98.3M.	ķ	8.5070	INCHES			I V	" "			9
## 9.3670 INCRES 2007		4.7460 INDES		0000	INCHES			2				200
# .01000 Mach No. 61/ 0 MA/L = 3.61 GRADIBNT INTERVAL = -5.00/ 5.00 Mach Math Meta		9.3670 INDES		0000	INDES			Æ		4.000		
ALPHA BETA & GF51) CN CAF CLM CBL CYN CY CY CY CY CAPPAG -5.000 0.00580 0.03500 0.03500 0.05580 0.05580 0.05580 0.03580 0.0558	4.4	0010.						1	{			
#### BETA & ##51) CN CAF CLM CBL CYN CY CY CY CY CY CAP CLM CBL CYN CY CY CAP			MAN NO.		н			-5.00/	3.6			
#### BETA & @*511 CM02536 .00692 .00560 .03500 .03500 .02536 .00692 .00560 .03500 .02530 .00620 .00660 .00660 .00660 .00660 .00693 .02593 .06593 .06593 .06593 .06593 .06593 .06593 .06593 .06593 .06594 .06760 .00660 .00669 .00691 .00693 .06593 .06593 .06594 .006961 .006961 .00698 .00688 .0068					i	910	3	ŧ	Ě	Շ	_	
#9.090 -5.00000 3.42295 .31030 .05799 .074240 .00020 .00366 .02993 .02993 .24.090 .00469 .02993 .24.090 -5.00000 3.42673 .66222 .0630707720 .00960 .00469 .0001100032 -	2		BETA	• 6 • 10	5	}	Arren -	26900	00000			2
24.880 -5.00000 3.42873 .66522 .0650702720 .00960 .00469 .0298100032 -	8.6		-9.00000	5.46285	- 500 A	05799	-,02480	02900	.00568			63
25.000 - 11000 - 05000 Airms Airms 5.000 - 100011 - 10005	9.6		-9.00000	3.53230	icoes.	TOR SOL	02720	09600	.00469			45
	9.9		-5.00000	3.42673	77600							ŗ

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DATE 21 JAM 74		F	ABLEATED	SOURCE DATA	, LARC 29	TABULATED SOURCE DATA, LARC 25 INCH HE-6441, (LA-15)	, (LA-15)			•	PAGE
			LA-15,RO	כנויברך 1980	ORB WAND	LA-15, ROCKLELL DOOR ONR WHOD NOSE W/O CHS (BANF)	(Buvf)		(RPH016)		(10 JAN 74)
PEPERENCE DATA	DATA							Ę	PARAMETRIC DATA	DATA	
LECT = 36,7360 56,114, LECT = 4,7460 INCRES BRCY = 9,3670 INCRES SCALE = ,0100		W H #	6.9070 INCHES .0000 INCHES .0000 INCHES	.9070 INCHES .0000 INCHES			BETA ATURON RUDFLR RN/L	K H H H	4.000 4.000 4.000	ELEVTR = RUDDER = RCHN95 =	10,000 ,000,
	RUN NO.	ġ	96.0	RMA = 3.75		CRADIENT INTERVAL =	-9.00/	3.00			
APPA 9,993 19,990 00,932 24,900 00,932 988.2 00,032 988.2	#TA -5,00000 - 5,00000 - 6,00000	8888	0(*51) 3,45131 3,45425 5,35150 .00803	90	.08478 .08113 .08807 .00133	0.4 02644 02716 00007	.00652 .00767 .00937	. 00571 . 00577 . 00458 00011	CY .03609 .03214 .03176 00043	-	CAB .00457 .00444 .00435
			LA-15,RC	113°00'	ON MANO	LA-15,NOCINELL DOGG CRB WATCO NOSE W/O CHS (BLAFF)	(BunF)		(1894017)	01)	(10 JAN 74)
ACTUBIONE DATA	E DATA							ζ.	PARAMETRIC DATA	DATA	
900 = 30,730 90,114. LICT = 4,740 INDES RICT = 9,3670 INDES SCALE : .0100	# 5 G	и и и	6.5070 .0000 .0000	6,5070 INDES ,0000 INDES ,0000 INDES			BETA A1LPO RUDFL RN/L	a	.000	ELEVTR = RUDDER = RGHPSS =	000°
	RUN NO.	õ	75/0	RV. = 3.90		GRADIENT INTERVAL =	5.00/ 5.00	9.00			
APAN POME 9.843 -19.850 9.843 -19.850 9.846 - 14.800 01.0 - 14.800 01.10	AT30 000000. 0000000. 0000000. 0000000. 000000	. 8 8 8 8 8	8.50057 3.59169 3.59169 3.59248 3.90600	04 - 47496 - 28273 - 27826 - 27436 - 19490	CAF .09789 .09233 .08436 .07659 .07200	62 (50 62 (50 62 (70 60 (70 60 60 (70 60 (70 60 (70 60 (70 60 (70 60 (70 60 (70.		CYN -,00031 -,00012 -,0004 -,00019 ,00019		17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	.00284 .00337 .00379 .00401 .00424

7 841 .6 24.44			TABULATED SOURCE DATA, LARC 20 INCH HE-6441, (LA-15)	RCE DATA,	LARC 20 IN	CH HE-6441,	(LA-15)			PAGE 8
			LA-15, ROCKWELL DOOD ORB W/HOD NOSE W/O OHS (BMNF)	ELL D898 OR	B W/MOD NO	SE W/O OHS	(BAVE)		(RPH018) ((10 JAN 74)
REFERENCE DATA	ece DAT	•						PARA	PARAMETRIC DATA	
2007 : 30,7360 50 LRCY : 4,7460 IN 10607 : 9,3470 IN	90. IN. INCIES INCIES	H day.Z	6,9070 INCHES ,DODO INCHES	INCIES INCIES INCIES			BETA AILRON RUGFLR RN/L		.000 RUDDER .000 RUDDER .000 RGPNSS .000 4.000	
		R NO.	76/ 0 RN/L =	3.82	GRADIENT INTERVAL	INTERVAL =	-9.00/	5.00		
9,940 -24,890 9,940 -24,890 5,940 -13,690 9,940 -9,890 9,940 -3,110	4 9. 0 0 9. 0 0 9. 0 0 9. 0 0. 0 0. 0 0. 0 0. 0 0. 0 0. 0 0. 0	META 	9.651) 3.66702 3.59199 5.49437 3.59778 3.00770	CN -, 519849 -, 37928 -, 19602 -, 13196	,12746 ,11263 ,09993 ,06669 ,06546	CLM 01727 C3804 04580 04433 03194 .00000	COL -,00096 -,00100 -,00126 -,00172 -,00172	CYN .00076 .00036 .00031 .00031	CY .00203 .00269 .00299 .00203	CAB , 00103 , 00256 , 00259 , 00361 , 00408
			LA-15, ROCK	LA-15, ROCKWELL DASA ONB WAYOD NOSE WAO ONS (BLAFF)	20 W/400 K	DE N/O CHS	(BunF)		(RPHC)19)	(10 JAN 74)
REFERE	REFERENCE DATA	4						PAR	PARAMETRIC DATA	
2007 = 30,7360 S LOGY = 4,746 II	sa. in. indes indes	# # # # # # # # # # # # # # # # # # #	6,5070 INCES ,0000 INCES	968 968 968			FETA ATLACN RUDFLR RN/L	3 c ć	5,000 ELEVTR ,000 RUDDER ,000 RGHNSS	
		PEN NO.	60/0 RNAL	L = 3.66	GRADIENT	GRADIENT INTERVAL =	-5.00/	5,00		
MACH ALPHA 2.940 -24.690 2.940 -11.690 2.940 - 09.690 09.6- 09.6	24.090 19.090 14.090	9.00000 9.00000 9.00000 9.00000 9.00000	9 (PS1) 3,57056 3,50076 3,47962 3,53667	ON 50486 39857 28767 19716 03170	.12630 .11477 .08997 .06749	CLM 02027 03611 04373 04315	CBL .01957 .01636 .01169 .00004	CYN .00694 .00305 00312 00604	.,11977 -,11977 -,10327 -,08749 -,07579	CAB ,00129 ,00227 ,00330 ,00387 ,00418
3	F	00000	00000	00000	00000	00000	CHOOCH.			